$\begin{tabular}{l} \hline \textbf{The nonlinear dynamics of ship motions: a field} \end{tabular}$ nonlinear dynamics of ship motions: a field
overview and some recent developments overview and some recent developments
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This opening article of the issue is intended to provide a review of the field of nonlin-This opening article of the issue is intended to provide a review of the field of nonlinear ship dynamics and to demonstrate the importance of the subject in the context of naval architecture. A list of relevant research t This opening article of the issue is intended to provide a review of the field of nonlinear ship dynamics and to demonstrate the importance of the subject in the context of naval architecture. A list of relevant research t ear ship dynamics and to demonstrate the importance of the subject in the context
of naval architecture. A list of relevant research topics that have received attention
in recent years is included in the first section of t of naval architecture. A list of relevant research topics that have received attention
in recent years is included in the first section of the paper. This sets the scene for
a brief discussion about the content and contrib in recent years is included in the first section of the paper. This sets the scene for
a brief discussion about the content and contribution of the articles that make up
the Theme Issue. In order to facilitate understandin a brief discussion about the content and contribution of the articles that make up
the Theme Issue. In order to facilitate understanding by non-specialists, we include
an outline of the general concepts of nonlinear dynami an outline of the general concepts of nonlinear dynamics. Furthermore, we provide a detailed review of the evolution of ship research of the considered type since the 1970s, including a rather lengthy bibliography. We discuss the latest ideas about ship capsize and we include a special section summarizing the recent advances with regard
to the mechanisms of ship capsize in astern seas. We close the article by offering some
ideas about future directions for research. to the mechanisms of ship capsize in astern seas. We close the article by offering some

Keywords: nonlinear; ship; bifurcation; chaos; capsize; broaching

1. Introduction

1. Introduction
In the field of nonlinear ship dynamics we explore the onset and evolution of the
unfamiliar and often unsafe dynamic responses beyond the linearity regime which In the field of nonlinear ship dynamics we explore the onset and evolution of the unfamiliar, and often unsafe, dynamic responses beyond the linearity regime, which are not amenable to the conventional techniques of seakee In the field of nonlinear ship dynamics we explore the onset and evolution of the unfamiliar, and often unsafe, dynamic responses beyond the linearity regime, which are not amenable to the conventional techniques of seakee unfamiliar, and often unsafe, dynamic responses beyond the linearity regime, which
are not amenable to the conventional techniques of seakeeping theory. The presence
of nonlinearity in the relation between excitation and r are not amenable to the conventional techniques of seakeeping theory. The presence
of nonlinearity in the relation between excitation and response in a dynamical system
creates the prospect of having multiple solutions for parameters. This could further lead to a plethora of very complicated phenomena creates the prospect of having multiple solutions for certain values of the system's
parameters. This could further lead to a plethora of very complicated phenomena
even when the type of nonlinearity is very simple; such a parameters. This could further lead to a plethora of very complicated phenomena
even when the type of nonlinearity is very simple; such as a quadratic or cubic term in
the stiffness component of an otherwise ordinary line the stiffness component of an otherwise ordinary linear driven oscillator (Thompson & Stewart 1986). Unexpected and violent transient motions leading to system escape, the stiffness component of an otherwise ordinary linear driven oscillator (Thompson & Stewart 1986). Unexpected and violent transient motions leading to system escape, irregular behaviour under regular excitation, subtle b & Stewart 1986). Unexpected and violent transient motions leading to system escape, irregular behaviour under regular excitation, subtle boundaries between the domains of coexisting responses, and sensitive dependence on i irregular behaviour under regular excitation, sub-
of coexisting responses, and sensitive dependence
known manifestations of nonlinear behaviour.
The above ideas are not yet fully domesticated of coexisting responses, and sensitive dependence on initial conditions are some well-
known manifestations of nonlinear behaviour.
The above ideas are not yet fully domesticated in naval architecture, a field that is

known manifestations of nonlinear behaviour.
The above ideas are not yet fully domesticated in naval architecture, a field that is
basically dominated by 'linear' concepts. However, nonlinear phenomena have been
found to u The above ideas are not yet fully domesticated in naval architecture, a field that is
basically dominated by 'linear' concepts. However, nonlinear phenomena have been
found to underlie ship dynamics in several instances, basically dominated by 'linear' concepts. However, nonlinear phenomena have been
found to underlie ship dynamics in several instances, much as they do for the dynamics of other engineering systems (Thompson $\&$ Bishop 19 ics of other engineering systems (Thompson & Bishop 1994; Moon 1999). Scientific
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1736 K . *J. Spyrou and J. M. T. Thompson*
curiosity apart, their particular engineering significance stems from their frequent
connection with safety-critical behaviour. For example, the roll stability of a ship curiosity apart, their particular engineering significance stems from their frequent
connection with safety-critical behaviour. For example, the roll stability of a ship
(the term stability used here in a liberal sense) is curiosity apart, their particular engineering significance stems from their frequent
connection with safety-critical behaviour. For example, the roll stability of a ship
(the term stability used here in a liberal sense) is (the term stability used here in a liberal sense) is considerably reduced once it is exposed to near resonant waves with steepness higher than some critical level. The reason is rapid loss of integrity of the domain of bounded (and thus safe) roll, due to a purely nonlinear mechanism. In other cases, variation of certain system parameters could suddenly render viable large motions with unusual characteristics. These varied parameters could either be representatives of the environment in which a ship operates, like the wave height and frequency, wind speed, etc., or they could reflect the ship's own operational and design characteristics, like the natural frequency and the damping in a direction of motion, the desired the ship's own operational and design characteristics, like the natural frequency and

By using the conceptual and computational framework of nonlinear dynamics, ship scientists around the world have recently produced some wonderful new insights into By using the conceptual and computational framework of nonlinear dynamics, ship scientists around the world have recently produced some wonderful new insights into phenomena of ship motion instability. An ensemble of 'geom scientists around the world have recently produced some wonderful new insights into
phenomena of ship motion instability. An ensemble of 'geometry-led' numerical and
analytical techniques has been the basis of these invest phenomena of ship motion instability. An ensemble of 'geometry-led' numerical and
analytical techniques has been the basis of these investigations, applied in conjunction
with mathematical models of various degrees of soph analytical techniques has been the basis of these investigations, applied in conjunction
with mathematical models of various degrees of sophistication. It is very encouraging
that descriptions of phenomena experienced in t that descriptions of phenomena experienced in the ocean by mariners often coincide closely with the theoretically predicted patterns. Research topics that have received particular attention recently are listed here.
(1) Ship capsize in regular 'beam' seas.

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- (1) Ship capsize in regular 'beam' seas.
(2) Development of transient capsize criteria based on Melnikov's method. (2) Development of transient capsize criteria b
(3) Criteria of ship capsize in random waves.
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- (3) Criteria of ship capsize in random waves.
(4) Large-amplitude rolling and capsize in longitudinal waves.
- (4) Large-amplitude rolling and capsize in longitudinal waves.

(5) Single-degree and coupled surge dynamics; especially the occurrence of asymmetric surging and surf-riding Single-degree and coupled surge
metric surging and surf-riding. metric surging and surf-riding.
(6) Broaching and its connection with capsize.
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- (7) Coupled rolling with liquid motion in an internal compartment.
- (7) Coupled rolling with liquid motion in an internal compartment.

(8) The behaviour of high-speed planing craft; especially the heave-pitch oscilla-

tions known as the porpoising condition The behaviour of high-speed planing craft
tions known as the porpoising condition.
- (9) Oscillations of moored, anchored or towed ships under the effects of currents (mainly for yaw motion) or waves (mainly for surge) Oscillations of moored, anchored or towed ships under (mainly for yaw motion) or waves (mainly for surge). (mainly for yaw motion) or waves (mainly for surge).
(10) Path control of marine vehicles and directional instability in strong wind.
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Some of these achievements will be reviewed below. Awareness of the fund of knowledge created by these investigations—combined with some familiarity, at a Some of these achievements will be reviewed below. Awareness of the fund of knowledge created by these investigations—combined with some familiarity, at a user level, with the techniques of nonlinear dynamics—will open new knowledge created by these investigations—combined with some user level, with the techniques of nonlinear dynamics—will open practising naval architects in their quest to maximize ship safety.
Increased computer power nowa Increased computer power nowadays allows us to carry out investigations on the sis of mathematical models featuring a considerable degree of detail. Indeed, one of

practising naval architects in their quest to maximize ship safety.
Increased computer power nowadays allows us to carry out investigations on the
basis of mathematical models featuring a considerable degree of detail. Ind basis of mathematical models featuring a considerable degree of detail. Indeed, one of the greatest challenges for the future will be interfacing, and, ultimately, integration, with the advances currently taking place in t the greatest challenges for the future will be interfacing, and, ultimately, integration, ics (Beck 1996; Huang & Sclavounos 1998). This will allow an explicit account of

the flow around ships' hulls and will supply the device for investigating the effect of the shape of the hull and the appendages on the nonlinear phenomena. Such an the flow around ships' hulls and will supply the device for investigating the effect
of the shape of the hull and the appendages on the nonlinear phenomena. Such an
optimistic view is somehow counterbalanced, however, by t the flow around ships' hulls and will supply the device for investigating the effect
of the shape of the hull and the appendages on the nonlinear phenomena. Such an
optimistic view is somehow counterbalanced, however, by t of the shape of the hull and the appendages on the nonlinear phenomena. Such an optimistic view is somehow counterbalanced, however, by the fact that the burden of identifying areas of critical behaviour becomes very consi identifying areas of critical behaviour becomes very considerable when the dynamical system is multi-dimensional (let alone when it is infinite dimensional, as is the identifying areas of critical behaviour becomes very considerable when the dynamical system is multi-dimensional (let alone when it is infinite dimensional, as is the true nature of the problem of a solid body's motion in ical system is multi-dimensional (let alone when it is infinite dimensional, as is the true nature of the problem of a solid body's motion in a fluid). The derivation of reduced-order approximations of the original system, reduced-order approximations of the original system, either through some rational dimension reduction procedure, or, merely, and usually more effectively, through insightful thinking, is very topical and will probably rema dimension reduction procedure, or, merely, and usually more effectively, through dimension reduction procedure, or, merely, and usually more effectively, through
insightful thinking, is very topical and will probably remain so because simple mod-
els are indispensable for developing an understanding ab insightful thinking, is very topical and will probably remain so because simple models are indispensable for developing an understanding about complex processes. To quote Wehausen (1979) in his tribute to Weinblum: 'a dire quote Wehausen (1979) in his tribute to Weinblum: 'a direct attack upon a too complicated problem may be in danger of not uncovering the underlying principles'. Much of the current interest in nonlinear ship dynamics was stirred by the success complicated problem may be in danger of not uncovering the underlying principles'.
Much of the current interest in nonlinear ship dynamics was stirred by the success
of the approach in unravelling, in a systematic way, the Much of the current interest in nonlinear ship dy
of the approach in unravelling, in a systematic way
behaviour on the basis of simple generic models. behaviour on the basis of simple generic models.
2. Content of the present Theme Issue

With the present Theme Issue we have attempted to present the various facets of ongoing research in the field. Contributions from the following areas have been included. (1) Investigations on instability phenomena based on simplified models.

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- (1) Investigations on instability phenomena based on simplified models.
(2) Criteria of nonlinear rolling and capsize in a random-wave environment.
- (2) Criteria of nonlinear rolling and capsize in a random-wave environme (3) Studies of nonlinear behaviour with detailed mathematical models. (3) Studies of nonlinear behaviour with detailed mathematical model (4) Observation and physical verification of complex behaviour.
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(4) Observation and physical verification of complex behaviour.
The first paper is from Jiang *et al*., and it is the latest addition to an impressive series of papers produced by 'the Michigan group' over the years on this subject. The first paper is from Jiang *et al.*, and it is the latest addition to an impressive
series of papers produced by 'the Michigan group' over the years on this subject.
In their present work they attempt to extend the Mel series of papers produced by 'the Michigan group' over the years on this subject.
In their present work they attempt to extend the Melnikov analysis applied for the
single-roll capsize problem in a random sea in order to i single-roll capsize problem in a random sea in order to include the so-called 'memory effect'. In many studies of nonlinear dynamics it has been quite common to assume single-roll capsize problem in a random sea in order to include the so-called 'memory
effect'. In many studies of nonlinear dynamics it has been quite common to assume
that the hydrodynamic force is only a function of the effect'. In many studies of nonlinear dynamics it has been quite common to assume
that the hydrodynamic force is only a function of the instantaneous ship motion. In a
strict sense this is not accurate, because, generally, that the hydrodynamic force is only a function of the instantaneous ship motion. In a
strict sense this is not accurate, because, generally, the whole history of motion plays
a role due to wave radiation from the ship's os strict sense this is not accurate, because, generally, the whole history of motion plays
a role due to wave radiation from the ship's oscillation and/or viscous effects. Taking
this feature into account would require inclu a role due to wave radiation from the ship's oscillation and/or viscous effects. Taking
this feature into account would require inclusion of convolution integrals leading to
an integrodifferential form of motion equations this feature into account would require inclusion of convolution integrals leading to
an integrodifferential form of motion equations and infinite-dimensional state space.
These authors have used the concept of phase space an integrodifferential form of motion equations and infinite-dimensional state space.
These authors have used the concept of phase space flux in their study, and they
approximated the memory effect through an auxiliary sys approximated the memory effect through an auxiliary system model, whose output represents an excitation to the original non-memory one. They have carried out the approximated the memory effect through an auxiliary system model, whose output
represents an excitation to the original non-memory one. They have carried out the
Melnikov analysis of the enlarged system and they have shown represents an excitation to the original non-memory one. They have carried out the Melnikov analysis of the enlarged system and they have shown some examples of how the memory term could influence the critical wave height Melnikov analysis of the enlarged system and they have shown some examples of
how the memory term could influence the critical wave height for capsize. Some
comparisons with non-memory models using constant characteristic how the memory term could influence the critical wave height for capsize. Some comparisons with non-memory models using constant characteristic frequencies are also presented. mparisons with non-memory models using constant characteristic frequencies are
so presented.
The work of Murashige *et al*. at the University of Tokyo deals with the problem
ship motion when some quantity of water exists i

also presented.
The work of Murashige *et al*. at the University of Tokyo deals with the problem
of ship motion when some quantity of water exists in an internal compartment. This
problem has received considerable attentio The work of Murashige *et al*. at the University of Tokyo deals with the problem of ship motion when some quantity of water exists in an internal compartment. This problem has received considerable attention recently beca *Phil. Trans. R. Soc. Lond.* A (2000)

chaos. These authors have carried out both numerical and experimental studies, and, despite a simple lumped-mass approach to the modelling of internal water movement, chaos. These authors have carried out both numerical and experimental studies, and, despite a simple lumped-mass approach to the modelling of internal water movement, the agreement between some of their findings (figures 2 despite a simple lumped-mass approach to the modelling of internal water movement,
the agreement between some of their findings (figures 2 and 13 of their paper) is
encouraging. They have used two different mathematical mo encouraging. They have used two different mathematical models, the simpler of which
has the form of a coupled Duffing's equation with a bistable restoring term and a encouraging. They have used two different mathematical models, the simpler of which
has the form of a coupled Duffing's equation with a bistable restoring term and a
nonlinear inertial matrix. An interesting account of the has the form of a coupled Duffing's equation with a bistable restoring term and a nonlinear inertial matrix. An interesting account of the occurring bifurcations is given. The authors also speculate that the cause of the c given. The authors also speculate that the cause of the chaotic responses is a chain of codimension-two bifurcations. Analyses of experimental data are presented in the paper, including data-smoothing techniques, phase-space reconstruction with delay time parameters, calculation of Lyapunov exponents, and paper, including data-smoothing techniques, phase-space reconstruction with delay dimension.

The paper of Spyrou of the National Technical University of Athens is an analysis of the coupled roll and surge dynamics. In steep following waves, the nonlinear features The paper of Spyrou of the National Technical University of Athens is an analysis of
the coupled roll and surge dynamics. In steep following waves, the nonlinear features
of the pendulum-like surge dynamics may become prev the coupled roll and surge dynamics. In steep following waves, the nonlinear features
of the pendulum-like surge dynamics may become prevalent, resulting in a motion
pattern in which the ship is spending more time near the of the pendulum-like surge dynamics may become prevalent, resulting in a motion
pattern in which the ship is spending more time near the crests of the waves than
near the troughs. However, as restoring is lowest around a c pattern in which the ship is spending more time near the crests of the waves than
near the troughs. However, as restoring is lowest around a crest, such a prolonged
stay at the crest can considerably influence the propensi stay at the crest can considerably influence the propensity for capsize. Inspired by this idea, the author has developed a new equation of roll motion in a following sea, which takes into account the surge dynamics. Another useful facet of this paper is the this idea, the author has developed a new equation of roll motion in a following sea, which takes into account the surge dynamics. Another useful facet of this paper is the demonstration of the layout of the stability tran which takes into account the surge dynamics. Another useful facet of this paper is the demonstration of the layout of the stability transition lines of the coupled system, which are contrasted with those of the ordinary Ma which are contrasted with those of the ordinary Mathieu-type system. In particular, the evolution of the capsize region in conjunction with the emergence of surf-riding. behaviour due to the occurrence of a homoclinic connection is very interesting. It seems that these phenomena tend to raise the probability of a quick capsize, and, therefore, their omission could result in underestimation seems that these phenomena tend to raise the probability of a quick capsize, and, ship.

The paper of Kreuzer & Wendt informs us about ongoing work at the Technical ship.
The paper of Kreuzer & Wendt informs us about ongoing work at the Technical
University of Hamburg–Harburg, where the main focus is the study of nonlinear
phenomena linked with ship capsize. The authors are using a fu The paper of Kreuzer & Wendt informs us about ongoing work at the Technical University of Hamburg–Harburg, where the main focus is the study of nonlinear phenomena linked with ship capsize. The authors are using a full si phenomena linked with ship capsize. The authors are using a full six-degrees-of-
freedom mathematical model with frequency-dependent hydrodynamic coefficients. A standard two-dimensional singularity method is used in the calculation of the freedom mathematical model with frequency-dependent hydrodynamic coefficients.
A standard two-dimensional singularity method is used in the calculation of the
hydrodynamic forces, while the inclusion of 'memory' has led to A standard two-dimensional singularity method is used in the calculation of the hydrodynamic forces, while the inclusion of 'memory' has led to a state-space representation with 164 degrees of freedom. Their investigations sentation with 164 degrees of freedom. Their investigations are carried out initially for a fixed rudder, but later they have used a proportional integral differential (PID) autopilot in order to control the rudder's movem for a fixed rudder, but later they have used a proportional integral differential (PID) for a fixed rudder, but later they have used a proportional integral differential (PID) autopilot in order to control the rudder's movement. They have presented animations of realistic ship behaviour in waves during capsiz autopilot in order to control the rudder's movement. They have present of realistic ship behaviour in waves during capsize in (stern) quarterin subharmonic and chaotic responses are identified in extreme waves.
The paper realistic ship behaviour in waves during capsize in (stern) quartering waves. Some
bharmonic and chaotic responses are identified in extreme waves.
The paper of Oh, Nayfeh & Mook from Virginia Tech describes the main find

subharmonic and chaotic responses are identified in extreme waves.
The paper of Oh, Nayfeh & Mook from Virginia Tech describes the main findings
of a combined theoretical and experimental investigation on indirectly excit The paper of Oh, Nayfeh & Mook from Virginia Tech describes the main findings of a combined theoretical and experimental investigation on indirectly excited rolling in head or following seas. Two specific phenomena are an of a combined theoretical and experimental investigation on indirectly excited rolling
in head or following seas. Two specific phenomena are analysed in detail: the first is a parametric resonance case in roll caused by the pitch and heave motions of a ship in waves. The equations describing heave and pitch are considered decoupled; however, the roll equation presents nonlinear couplings with both of these motions. The main safety-related finding here is the discovery of a subcritical pitchfork bifurcation and it is very notable that its existence was confirmed during experiments with a model ship. Another case analysed in this paper is autoparametric resonance for coupled pitch and roll. Again dangerous subcritical-type instability phenomena were found. This paper shows that it is certainly possible to correla pitch and roll. Again dangerous subcritical-type instability phenomena were found.

the results of model experiments, despite the complex character of the behaviour and the many parameters that are involved in such experiments.

Umeda & Hamamoto of Osaka University have collected some very interesting the many parameters that are involved in such experiments.
Umeda & Hamamoto of Osaka University have collected some very interesting
visual images of ship behaviour in connection with four different capsize modes in
high-s Umeda & Hamamoto of Osaka University have collected some very interesting
visual images of ship behaviour in connection with four different capsize modes in
high-stern-quartering seas. These images were obtained during exp high-stern-quartering seas. These images were obtained during experiments based on radio-controlled models. The experiments were carried out at the Marine Dynamics high-stern-quartering seas. These images were obtained during experiments based on radio-controlled models. The experiments were carried out at the Marine Dynamics Basin of the National Research Institute of Fisheries Engi radio-controlled models. The experiments were carried out at the Marine Dynamics
Basin of the National Research Institute of Fisheries Engineering of Japan. The
authors have reproduced capsize according to two less frequen authors have reproduced capsize due to broaching and due to parametric instability.
Also, they have shown capsize according to two less frequently discussed modes:
capsize after bow diving; and capsize due to a kind of pur Also, they have shown capsize according to two less frequently discussed modes: involved.

The final contribution featuring model experiments comes from Ikeda $&$ Katayama involved.
The final contribution featuring model experiments comes from Ikeda & Katayama
of the University of Osaka Prefecture and is focused on ship behaviour at high speed.
These authors have studied the onset of the so The final contribution featuring model experiments comes from Ikeda & Katayama
of the University of Osaka Prefecture and is focused on ship behaviour at high speed.
These authors have studied the onset of the so-called po of the University of Osaka Prefecture and is focused on ship behaviour at high speed.
These authors have studied the onset of the so-called porpoising oscillations (self-
sustained pitch and heave) for a marine craft with These authors have studied the onset of the so-called porpoising oscillations (self-
sustained pitch and heave) for a marine craft with spray rails operating up to a Froude
number as high as 6.0. On the basis of a one-quar number as high as 6.0. On the basis of a one-quarter-scale model they measured the forces with captive tests for various running attitudes and speeds, and they found number as high as 6.0. On the basis of a one-quarter-scale model they measured the
forces with captive tests for various running attitudes and speeds, and they found
nonlinearity for heave and pitch restoring at high speed forces with captive tests for various running attitudes and speeds, and they found
nonlinearity for heave and pitch restoring at high speed, especially for the cross-
coupling terms. This information was introduced into a coupling terms. This information was introduced into a mathematical model in order to simulate the initial occurrence and further build-up of porpoising. The derived predictions of porpoising characteristics were compared with direct experimental measurements and found to be in good agreement. predictions of porpoising characteristics were compared with direct experimental

The last three contributions are concerned with the characteristics of nonlinear measurements and found to be in good agreement.
The last three contributions are concerned with the characteristics of nonlinear
rolling in a random seaway. Roberts $\&$ Vasta of the University of Sussex have applied
an a The last three contributions are concerned with the characteristics of nonlinear
rolling in a random seaway. Roberts $\&$ Vasta of the University of Sussex have applied
an averaging procedure, showing that, under certain an averaging procedure, showing that, under certain conditions, the energy envelope of the roll response can be modelled as a continuous Markov process. Their approach could be useful for deriving probability density functions of roll response when the time to capsize is very long. Another potential use of this work is in the derivation of damping and excitation data from the so-called d time to capsize is very long. Another potential use of this work is in the derivation calculated on the basis of actual ship roll-response information.

The papers of Senjanović and Falzarano with their associates are more mainstream nonlinear-dynamics investigations of ship capsize under stochastic wave excitation. These works are highly complementary, as they seem to approach the same problem monlinear-dynamics investigations of ship capsize under stochastic wave excitation.
These works are highly complementary, as they seem to approach the same problem
from a different perspective. Senjanović, Ciprić & Parunov These works are highly complementary, as they seem to approach the same problem
from a different perspective. Senjanović, Ciprić & Parunov from the University of
Zagreb followed a repetitive simulation procedure in order from a different perspective. Senjanović, Ciprić & Parunov from the University of Zagreb followed a repetitive simulation procedure in order to produce a chart giving the probability of capsize (for a certain wave spectru Zagreb followed a repetitive simulation procedure in order to produce a chart giving
the probability of capsize (for a certain wave spectrum) in terms of ship-motion
direction and speed. As usual, they have derived the (ir the probability of capsize (for a certain wave spectrum) in terms of ship-motion
direction and speed. As usual, they have derived the (irregular) wave forcing by
a sum of a finite number of harmonic wave components with r direction and speed. As usual, they have derived the (irregular) wave forcing by
a sum of a finite number of harmonic wave components with random phases. As
the detailed form of the righting-arm (GZ) -curve is taken into the detailed form of the righting-arm (GZ) -curve is taken into account, this chart could be used also for linking quantitatively the shape of the (GZ) -curve with the probability of capsize. could be used also for linking quantitatively the shape of the (GZ) -curve with the uld be used also for linking quantitatively the shape of the (GZ) -curve with the obability of capsize.
Instead of performing many simulations, Vishnubhotla with Falzarano (Univer-
v of New Orleans) and Vakakis (Universit

probability of capsize.
Instead of performing many simulations, Vishnubhotla with Falzarano (University of New Orleans) and Vakakis (University of Illinois at Urbana) attempted to
derive approximate analytical expressions sity of New Orleans) and Vakakis (University of Illinois at Urbana) attempted to derive approximate analytical expressions for the inset and outset of the hill-top saddle under pseudo-random-wave excitation. They used tech derive approximate analytical expressions for the inset and outset of the hill-top derive approximate analytical expressions for the inset and outset of the hill-top
saddle under pseudo-random-wave excitation. They used techniques from the theory
of rapidly varying excitations and they applied for a cubi saddle under pseudo-random-wave excitation. They used techniques from the theory
of rapidly varying excitations and they applied for a cubic-type restoring function
whose Hamiltonian manifold solution is well known. The an whose Hamiltonian manifold solution is well known. The analytical approach could have some problems for more realistic higher-order restoring polynomials; however,

1. Evolution of steady-state responses for increasing excitation bas a roll equation allowing only one-sided escape (Thompson 1996).

a roll equation allowing only one-sided escape (Thompson 1996).
the authors believe that the numerical route could be applied without problems in
these cases. the authors b
these cases.

3. Introductory aspects of nonlinear dynamics

3. Introductory aspects of nonlinear dynamics
A simple, harmonically forced oscillator with a quadratic 'softening' nonlinearity in
restoring has been used as a generic model for studying various physical phenomena A simple, harmonically forced oscillator with a quadratic 'softening' nonlinearity in
restoring has been used as a generic model for studying various physical phenomena,
one being one-sided ship capsize in 'beam' waves (Th A simple, harmonically forced oscillator with a quadratic 'softening' nonlinearity in restoring has been used as a generic model for studying various physical phenomena, one being one-sided ship capsize in 'beam' waves (Th restoring has been used as a generic model for studying various physical phenomena,
one being one-sided ship capsize in 'beam' waves (Thompson 1997). The evolution of
the responses as the forcing is stepped up amply demons one being one-sided ship capsize in 'beam' waves (Thompson 1997). The evolution of
the responses as the forcing is stepped up amply demonstrates several characteristic
features of nonlinear systems (figure 1). Most familia the responses as the forcing is stepped up amply demonstrates several characteristic
features of nonlinear systems (figure 1). Most familiar are the 'skewed' (to the left
for softening nonlinearity) frequency-response curv for softening nonlinearity) frequency-response curve and the gradual appearance of higher harmonics 'distorting' the ordinary harmonic motion. At a certain level of forcing, the effect of nonlinearity becomes so drastic on higher harmonics 'distorting' the ordinary harmonic motion. At a certain level of higher harmonics 'distorting' the ordinary harmonic motion. At a certain level of forcing, the effect of nonlinearity becomes so drastic on the upper limb that the original response turns unstable with a stable subharmonic forcing, the effect of nonlinearity becomes so drastic on the upper limb that the original response turns unstable with a stable subharmonic emerging. Qualitative changes in the character of behaviour are manifestations of changes in the character of behaviour are manifestations of *bifurcations*, which are very common phenomena in nonlinear systems. They can be realized according to changes in the character of behaviour are manifestations of *bifurcations*, which are
very common phenomena in nonlinear systems. They can be realized according to
a small number of generic patterns, which may involve smoo very common phenomen
a small number of gener
towards another state.
The discovery and in-Small number of generic patterns, which may involve smooth or abrupt transition
wards another state.
The discovery and in-depth study of bifurcations are key tasks in the exploration
ship dynamics. The robustness of the bi

towards another state.
The discovery and in-depth study of bifurcations are key tasks in the exploration
of ship dynamics. The robustness of the bifurcations in variations of the mathemat-The discovery and in-depth study of bifurcations are key tasks in the exploration
of ship dynamics. The robustness of the bifurcations in variations of the mathemat-
ical model allows us to draw certain conclusions about of ship dynamics. The robustness of the bifurcations in variations of the mathematical model allows us to draw certain conclusions about the behaviour of the system without necessarily having a complete mathematical model without necessarily having a complete mathematical model (almost universally the case when studying extreme ship motions in waves). This property could be exploited during free-running ship model tests in large waves, where making direct comparisons between theory and experiment is non-trivial, as the number of unknowns is very large and some of the parameters are practically non-cont isons between theory and experiment is non-trivial, as the number of unknowns is imum number of system ('control') parameters that render a bifurcation robust

Figure 2. Codimension-one local bifurcations: (i) flip, (ii) pitchfork. Both of these may appear Figure 2. Codimension-one local bifurcations: (i) flip, (ii) pitchfork. Both of these may appear
as: (iii) supercritical, or (iv) subcritical. Other possible bifurcations are: (v) the folds, (vi) super-
critical Hopf and (Figure 2. Codimension-one local biturcat
as: (iii) supercritical, or (iv) subcritical. O
critical Hopf and (vii) subcritical Hopf.

(contributed Hopf and (vii) subcritical Hopf.

('structurally stable') determines the *codimension* of this bifurcation. Bifurcation ('structurally stable') determines the *codimension* of this bifurcation. Bifurcation phenomena are generally classified as local or global. Local bifurcation phenomena correspond to the creation disappearance or change i ('structurally stable') determines the *codimension* of this bifurcation. Bifurcation
phenomena are generally classified as local or global. Local bifurcation phenomena
correspond to the creation, disappearance or change phenomena are generally classified as local or global. Local bifurcation phenomena
correspond to the creation, disappearance or change in stability of a steady-state
solution. Local, codimension-1 bifurcations are the fold correspond to the creation, disappearance or change in stability of a steady-state
solution. Local, codimension-1 bifurcations are the fold (also known as the saddle-
node bifurcation, turning point or limit point), the pi solution. Local, codimension-1 bifurcations are the fold (also known as the saddle-
node bifurcation, turning point or limit point), the pitchfork, the flip (period dou-
bling), and the Hopf bifurcation (figure 2). All the mode bifurcation, turning point or limit point), the pitchfork, the flip (period doubling), and the Hopf bifurcation (figure 2). All these have confirmed relevance to ship motions. Of particular interest for engineering sy bling), and the Hopf bifurcation (figure 2). All these have confirmed relevance to ship
motions. Of particular interest for engineering systems are those bifurcations that
do not create a stable state in the vicinity past motions. Of particular interest for engineering systems are those bifurcations that
do not create a stable state in the vicinity past the bifurcation point. At a fold, no
solution exists at all, and a jump towards some dis do not create a stable state in the vicinity past the bifurcation point. At a fold, no solution exists at all, and a jump towards some distant state or even towards infinity becomes inevitable. A similarly dangerous jump w solution exists at all, and a jump towards some distant state or even towards infinity
becomes inevitable. A similarly dangerous jump will arise at a pitchfork, flip or Hopf
bifurcation if these are of a *subcritical* type becomes inevitable. A similarly dangerous jump will arise at a pitchfork
bifurcation if these are of a *subcritical* type. A classification of generic
for dissipative dynamical systems is given in Thompson *et al.* (1994). bifurcation if these are of a *subcritical* type. A classification of generic bifurcations for dissipative dynamical systems is given in Thompson *et al.* (1994).
However, the study of bifurcations in a steady-state sense

for dissipative dynamical systems is given in Thompson *et al.* (1994).
However, the study of bifurcations in a steady-state sense does not offer a complete
account of nonlinear behaviour. Unsafe transitions are, by their However, the study of bifurcations in a steady-state sense does not offer a complete
account of nonlinear behaviour. Unsafe transitions are, by their very nature, extreme
unsteady phenomena. Also, in the continually changi unsteady phenomena. Also, in the continually changing conditions of the ocean, a ship will only rarely operate in a steady condition. The level of excitation required
for system escape during a transient is lower than that of the steady state, and, thus,
safety-margin predictions based on steady states ship will only rarely operate in a steady condition. The level of excitation required
for system escape during a transient is lower than that of the steady state, and, thus,
safety-margin predictions based on steady states for system escape during a transient is lower than that of the steady state, and, thus, safety-margin predictions based on steady states could overestimate the true safety margin. The assessment of critical behaviour requi margin. The assessment of critical behaviour requires, therefore, some understanding
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of the principles governing transient motions. Generally, such an understanding can be acquired more easily if a geometric approach is adopted in which the motions' of the principles governing transient motions. Generally, such an understanding can
be acquired more easily if a geometric approach is adopted in which the motions'
characteristics are studied in the so-called phase (or st be acquired more easily if a geometric approach is adopted in which the motions'
characteristics are studied in the so-called phase (or state) space, or through its two-
dimensional projections. The phase space is basicall dimensional projections. The phase space is basically an enlarged physical space.
Its dimension is determined by the number of initial conditions required in order dimensional projections. The phase space is basically an enlarged physical space.
Its dimension is determined by the number of initial conditions required in order
to obtain, from the motion equations, a unique solution in Its dimension is determined by the number of initial conditions required in order
to obtain, from the motion equations, a unique solution in time. In the case of
undriven rolling, for example, it suffices to know the init undriven rolling, for example, it suffices to know the initial roll angle (i.e. the value at $t=0$) and the initial roll velocity, in order to determine the solution at a later time instant; so the state-space dimension is, in this case, 2. The continuous time evolution of a solution produces a *trajectory* (also called an *orbit*). Such trajectories cannot cross in phase space; otherwise, at the intersection point there would exist non-unique evolution. Stationary steady solut cannot cross in phase space; otherwise, at the intersection point there would exist cannot cross in phase space; otherwise, at the intersection point there would exist
non-unique evolution. Stationary steady solutions are represented in state space by
points, while periodic solutions appear as closed curv *attractors* (or *sinks*) because the trajectories starting from nearby points, while periodic solutions appear as closed curves. Stable solutions are called *attractors* (or *sinks*) because the trajectories starting from points, while periodic solutions appear as closed curves. Stable solutions are called *attractors* (or *sinks*) because the trajectories starting from nearby points tend to end on these. The unstable solutions are called attractors (or *sinks*) because the trajectories starting from nearby points tend to
end on these. The unstable solutions are called *repellers* (or *sources*). Quite often we
may have attraction in certain directions and end on these. The unstable solutions are called *repellers* (or *sources*). Quite often we
may have attraction in certain directions and repulsion in the others. This is the case
of *saddle*. The evolution of initial condi may have attraction in certain directions and repulsion in the others. This is the case
of *saddle*. The evolution of initial conditions produces a flow in phase space. When
the steady response contains incommensurate freq of *saddle*. The evolution of initial conditions produces a flow in phase space. When
the steady response contains incommensurate frequencies we have a *quasi-periodic*
attractor or repeller ('leaving' on a torus). In some the steady response contains incommensurate frequencies we have a *quasi-periodic* attractor or repeller ('leaving' on a torus). In some cases the response is characterized by broad-band noise and extreme sensitivity to in by broad-band noise and extreme sensitivity to initial conditions, despite the fact that the system is forced regularly. This is the case of a *chaotic* response. Typical routes to chaos are through a cascade of period-doubling bifurcations, as exhibited in figure 1 (the ratio of the distance between successive bifurcation frequencies converges to the universal constant 4.669, first discove routes to chaos are through a cascade of period-doubling bifurcations, as exhibited in
figure 1 (the ratio of the distance between successive bifurcation frequencies converges
to the universal constant 4.669, first discov figure 1 (the ratio of the distance between successive bifurcation frequencies converges
to the universal constant 4.669, first discovered by Feigenbaum); through quasi-
periodicity and through intermittency (Bergé *et al.* to the universal constant 4.669, first discovered by Feigenbaum); through quasi-
periodicity and through intermittency (Bergé *et al.* 1984). The first two routes have
been discussed in the context of ship motions (Virgin periodicity and through intermittency (Bergé *et al.*)
been discussed in the context of ship motions (Vi
1991; Spyrou 1996b; Murashige & Aihara 1998a).
A key concept required for the study of transients en discussed in the context of ship motions (Virgin 1987; Rainey & Thompson 91; Spyrou 1996*b*; Murashige & Aihara 1998*a*).
A key concept required for the study of transients is the *basin* (*domain*) of attrac-
on rep

1991; Spyrou 1996*b*; Murashige & Aihara 1998*a*).
 A key concept required for the study of transients is the *basin* (*domain*) of attraction, representing the set of initial conditions that lead to a certain attractor A key concept required for the study of transients is the *basin* (*domain*) of attraction, representing the set of initial conditions that lead to a certain attractor for fixed control parameters' settings. Conversely, t fixed control parameters' settings. Conversely, the basin of attraction may also be defined in the control space for fixed initial conditions. For a simple two-dimensional fixed control parameters' settings. Conversely, the basin of attraction may also be defined in the control space for fixed initial conditions. For a simple two-dimensional system the boundary of the basin of attraction is defined in the control space for fixed initial conditions. For a simple two-dimensional
system the boundary of the basin of attraction is determined by those special orbits
that approach (in infinite time) nearby saddle-ty system the boundary of the basin of attraction is determined by those special orbits
that approach (in infinite time) nearby saddle-type states (figure 3). Together with
their 'twin' orbits, which leave these saddles, they that approach (in infinite time) nearby saddle-type states (figure 3). Together with their 'twin' orbits, which leave these saddles, they are usually called *invariant manifolds*, or, more correctly, *inset* (if entering a $folds,$ or, more correctly, *inset* (if entering a saddle) and *outset* (if leaving a saddle). boundaries that are not sharp. The critical event leading to such a development is These manifolds can sometimes become entangled in a very intricate way, producing
boundaries that are not sharp. The critical event leading to such a development is
the tangency of a pair of manifolds originating from the boundaries that are not sharp. The critical event leading to such a development is
the tangency of a pair of manifolds originating from the same ('homoclinic') or from
different ('heteroclinic') saddles. This is a *global* the tangency of a pair of manifolds originating from the same ('homoclinic') or from
different ('heteroclinic') saddles. This is a *global bifurcation* phenomenon creating a
major phase-space rearrangement (figure 3). Such different ('heteroclinic') saddles. This is a *global bifurcation* phenomenon creating a
major phase-space rearrangement (figure 3). Such phenomena are very critical for
the system's integrity because they are associated w major phase-space rearrangement (figure 3). Such phenomena are very critical for
the system's integrity because they are associated with rapid loss from within the
area of the safe basin (figure 4). They also generate tran the system's integrity because they are associated with rapid loss from within the area of the safe basin (figure 4). They also generate transient chaos: orbits started at certain initial conditions wander in an apparently area of the safe basin (figure 4). They also generate transient chaos: orbits started
at certain initial conditions wander in an apparently random manner, albeit that
they settle to a repeating pattern in the long term. Fu at certain initial conditions wander in an apparently random manner, albeit that they settle to a repeating pattern in the long term. Further stepping-up of a critical control parameter, however, such as the forcing amplit control parameter, however, such as the forcing amplitude, is likely to create chaos

Heteroclinic/homoclinic tangencies have been linked to the process of ship capsize in resonant beam seas (Thompson & Soliman 1990). Their occurrence can be pre-

Figure 3. Global bifurcations with known relevance for ship dynamics.
(a) Homoclinic tangency in a map; (b) homoclinic saddle connection.

Equal that is dependence of the exponent of the (Thompson & Soliman 1990).

(Thompson & Soliman 1990).
dicted either numerically or, in an approximate sense, analytically. The analytical
route has been very popular in the recent past, and is based on the so-called Melnikov dicted either numerically or, in an approximate sense, analytically. The analytical
route has been very popular in the recent past, and is based on the so-called Melnikov
method of analytical mechanics, which in a strict s dicted either numerically or, in an approximate sense, analytically. The analytical route has been very popular in the recent past, and is based on the so-called Melnikov method of analytical mechanics, which, in a strict route has been very popular in the recent past, and is based on the so-called Melnikov method of analytical mechanics, which, in a strict sense, is valid only for infinitesimal damping (e.g. Guckenheimer $\&$ Holmes 1983) *Phil. Trans. R. Soc. Lond.* A (2000) *Phil. Trans. R. Soc. Lond.* A (2000)

tegrity contours for the 'one-sided-escape' equation. Rem area shown as a percentage, $\beta = 0.1$ (Thompson 1996). area shown as a percentage, $\beta = 0.1$ (Thompson 1996).
is to express the distance between the critical pair of manifolds as a function of the

is to express the distance between the critical pair of manifolds as a function of the ship and environmental parameters. Then, by setting this distance to zero, we can determine the critical combination of these parameter is to express the distance between the critical pair of manifolds as a function of the ship and environmental parameters. Then, by setting this distance to zero, we can determine the critical combination of these parameter determine the critical combination of these parameters. This condition is equivalent, with a balancing of the energy coming in through forcing with the energy dissipated determine the critical combination of these parameters. This condition is equivalent,
with a balancing of the energy coming in through forcing with the energy dissipated
through damping, for the remotest bounded orbit (for with a balancing of the energy coming in through forcing with the energy dissipated
through damping, for the remotest bounded orbit (for a Hamiltonian system, this
is the homoclinic one). The bifurcation diagram of the sim through damping, for the remotest bounded orbit (for a Hamiltonian system, this
is the homoclinic one). The bifurcation diagram of the simple oscillator of figure 1
including the Melnikov curve as well as the numerical pre is the homoclinic one). The bifure
including the Melnikov curve as
connection is shown in figure 5.
Another type of global bifurcat cluding the Melnikov curve as well as the numerical prediction of the homoclinic
nection is shown in figure 5.
Another type of global bifurcation that has manifested itself in ship dynamics is
e so-called *homoclinic saddl*

the so-called *homoclinic saddle connection*, which is a dangerous 'blue-sky' event. A saddle 'approaches' an existing stable periodic orbit until there is contact (equiv-Another type of global bifurcation that has manifested itself in ship dynamics is
the so-called *homoclinic saddle connection*, which is a dangerous 'blue-sky' event. A
saddle 'approaches' an existing, stable, periodic orb the so-called *homoclinic saddle connection*, which is a dangerous 'blue-sky' event. A saddle 'approaches' an existing, stable, periodic orbit until there is contact (equivalently, an inset-outset pair of the saddle touche alently, an inset-outset pair of the saddle touches the periodic orbit tangentially).
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The outcome is the sudden disappearance of the periodic orbit from phase space The outcome is the sudden disappearance of the periodic orbit from phase space (figure 3). Such an event has been identified to be behind the so-called *surf-riding* condition, and it is the main cause of *broaching* (Spy The outcome is the sudden disappearance of the periodic orbit i
(figure 3). Such an event has been identified to be behind the so-
condition, and it is the main cause of *broaching* (Spyrou 1996a).
It is quite straightforw gure 3). Such an event has been identified to be behind the so-called *surf-riding* ndition, and it is the main cause of *broaching* (Spyrou 1996*a*). It is quite straightforward to identify basins of attraction and extra

condition, and it is the main cause of *broaching* (Spyrou 1996*a*).
It is quite straightforward to identify basins of attraction and extract the phase-
space organization through discretization of the phase space and dir It is quite straightforward to identify basins of attraction and extract the phase-
space organization through discretization of the phase space and direct integration
from the nodes of a dense grid of initial conditions. space organization through discretization of the phase space and direct integration
from the nodes of a dense grid of initial conditions. A more efficient, computationally,
version of this method is the cell-to-cell mappin from the nodes of a dense grid of initial conditions. A more efficient, computationally,
version of this method is the cell-to-cell mapping technique, which ensures that points
whose evolution is known are not examined rep whose evolution is known are not examined repetitively (Hsu 1987). These methods are generally very successful for two-dimensional Poincaré sections (a Poincaré section is basically a section through phase space transverse are generally very successful for two-dimensional Poincaré sections (a Poincaré secare generally very successful for two-dimensional Poincaré sections (a Poincaré sec-
tion is basically a section through phase space transverse to the flow that allows the
study of the dynamics on a plane), but their effic tion is basically a section through phase space transverse to the flow that allows the study of the dynamics on a plane), but their efficiency falls quickly as the phase-
space dimension is increased. For example, for a ty study of the dynamics on a plane), but their efficiency falls quickly as the phase-
space dimension is increased. For example, for a typical 12-dimensional phase space
required for the general study of ship dynamics in al space dimension is increased. For example, for a typical 12-dimensional phase space
required for the general study of ship dynamics in all six degrees of freedom and
a modest grid density of 300 nodes in each direction, s a modest grid density of 300 nodes in each direction, simulations for 300^{12} points would be needed! More intelligent searching techniques are therefore required. The analysis of multi-degree-of-freedom systems is a new field still under development.

4. Historical note on nonlinear ship dynamics

4. Historical note on nonlinear ship dynamics
The forerunners of the modern approaches are traced back to the 1970s: Zeeman's
(1977) reformulation of some classical results of roll stability from the perspective of The forerunners of the modern approaches are traced back to the 1970s: Zeeman's
(1977) reformulation of some classical results of roll stability from the perspective of
catastrophe theory bears a strong resemblance to many (1977) reformulation of some classical results of roll stability from the perspective of catastrophe theory bears a strong resemblance to many of the popular geometrical (1977) reformulation of some classical results of roll stability from the perspective of catastrophe theory bears a strong resemblance to many of the popular geometrical approaches used today (see also Poston & Stewart 19 catastrophe theory bears a strong resemblance to many of the popular geometrical
approaches used today (see also Poston & Stewart 1978). In the 1970s, the study of
large-amplitude rolling in beam waves became topical, perh large-amplitude rolling in beam waves became topical, perhaps due to the SAFESHIP
project funded by the UK government. Analytical approximations of the steady-state large-amplitude rolling in beam waves became topical, perhaps due to the SAFESHIP
project funded by the UK government. Analytical approximations of the steady-state
rolling response with higher harmonics were derived by ap project funded by the UK government. Analytical approximations of the steady-state rolling response with higher harmonics were derived by applying the asymptotic, the harmonic balance, and other perturbation-based methods rolling response with higher harmonics were derived by applying the asymptotic, the harmonic balance, and other perturbation-based methods (Odabashi 1973; Wellicome 1975; Wright & Marshfield 1980). In these studies, roll w harmonic balance, and other perturbation-based methods (Odabashi 1973; Wellicome 1975; Wright & Marshfield 1980). In these studies, roll was uncoupled and the waves were considered long compared with the ship's beam, resul 1975; Wright & Marshfield 1980). In these studies, roll was uncoupled and the waves
were considered long-compared with the ship's beam, resulting in a mathematical
model that is basically a classical Duffing-type forced o were considered long compared with the ship's beam, resulting in a mathematical model that is basically a classical Duffing-type forced oscillator with a single potential well. Actually, these were not the first explorations of the nonlinear roll equation; for example, Baumann (1955) nicely demonstrated the dependence of the shape of the frequency-response curve on the form of realistic $(G$ example, Baumann (1955) nicely demonstrated the dependence of the shape of the

Marsh field (1978) published the first results of the well-known 'Admiralty model frequency-response curve on the form of realistic (GZ) -functions.
Marshfield (1978) published the first results of the well-known 'Admiralty model
tests', providing concrete evidence about the nonlinear character of the Marshfield (1978) published the first results of the well-known 'Admiralty model
tests', providing concrete evidence about the nonlinear character of the frequency-
response curve and the existence of bistability in a cert response curve and the existence of bistability in a certain range around resonance (see also Marshfield 1987). Records of subharmonic responses were also presented, verifying that the roll motion may undergo a period-doubling bifurcation. Analyti-(see also Marshfield 1987). Records of subharmonic responses were also presented, verifying that the roll motion may undergo a period-doubling bifurcation. Analytical investigations on subharmonic rolling were performed l verifying that the roll motion may undergo a period-doubling bifurcation. Analytical investigations on subharmonic rolling were performed later by the Trieste group (Cardo *et al.* 1981). Marshfield has also made the impor cal investigations on subharmonic rolling were performed later by the Trieste group
(Cardo *et al.* 1981). Marshfield has also made the important observation that the
existence of bias towards and away from the wave sourc (Cardo *et al.* 1981). Marshfield has also made the important observation that the existence of bias towards and away from the wave source produces different results in terms of capsize; and that the unbiased model shows existence of bias towards and away from the wave source produces different results in terms of capsize; and that the unbiased model shows a tendency to capsize towards the wave source. Sway coupling may be necessary for explaining these tendencies, the wave source. Sway coupling may be necessary for explaining these tendencies,
but roll is quite often studied uncoupled. Some simplifying assumptions about the
roll centre are necessary in order to justify this model (H but roll is quite often studied uncoupled. Some simplifying assumptions about the roll centre are necessary in order to justify this model (Hutchison 1990). It is quite common to describe the roll motion on the basis of th roll centre are necessary in order to justify this model (Hutchison 1990). It is quite common to describe the roll motion on the basis of the relative roll angle as measured from the local wave slope. Of course, the absol common to describe the roll motion on the basis of the relative roll angle as measured

1998). Analytical studies of steady rolling in beam seas continue to be carried out up to the present day (Senjanović 1994; Peyton Jones & Cancaya 1997). 98). Analytical studies of steady rolling in beam seas continue to be carried out
to the present day (Senjanović 1994; Peyton Jones & Cancaya 1997).
Odabashi seemed to be the first person to make the connection with the c

up to the present day (Senjanović 1994; Peyton Jones & Cancaya 1997).

Odabashi seemed to be the first person to make the connection with the classi-

cal theory of stability, recognizing that the domain of attraction, rat cal theory of stability, recognizing that the domain of attraction, rather than the steady-state, holds the key to the assessment of ship safety against capsize. He proposed the derivation of criteria for ensuring the boundedness of roll motion through steady-state, holds the key to the assessment of ship safety against capsize. He proposed the derivation of criteria for ensuring the boundedness of roll motion through the analytical construction of the so-called Lyapunov posed the derivation of criteria for ensuring the boundedness of roll motion through
the analytical construction of the so-called Lyapunov functions (Kuo & Odabashi
1975; Odabashi 1977, 1978, 1982). These Lyapunov function 1975; Odabashi 1977, 1978, 1982). These Lyapunov functions were hotly debated in the 1970s and 1980s in the naval architectural community, which was perhaps still unprepared for adopting such highly mathematical techniques 1975; Odabashi 1977, 1978, 1982). These Lyapunov functions we
the 1970s and 1980s in the naval architectural community, whice
unprepared for adopting such highly mathematical techniques.
In the United States. Navfeh *et a* 1970s and 1980s in the naval architectural community, which was perhaps still
prepared for adopting such highly mathematical techniques.
In the United States, Nayfeh *et al.* (1973) published a paper about nonlinearly
uple

unprepared for adopting such highly mathematical techniques.
In the United States, Nayfeh *et al.* (1973) published a paper about nonlinearly coupled pitch and roll using the method of multiple scales. In head seas, direc In the United States, Nayfeh *et al.* (1973) published a paper about nonlinearly coupled pitch and roll using the method of multiple scales. In head seas, directly excited pitch can create growth of roll, which will influe excited pitch can create growth of roll, which will influence back pitch, and so forth. A critical development is the saturation of the pitch response and the transfer of all the energy that enters the pitch mode into roll. As stated in their introduction, the authors had been inspired by Froude's (1863) observation, published in his discussion
of Scott Russel's paper at the Institution of Naval Architects, that ships present
undesirable roll characteristics when the natural fre of Scott Russel's paper at the Institution of Naval Architects, that ships present of roll. Sethna & Bajaj (1978) predicted further amplitude-modulated motions in undesirable roll characteristics when the natural frequency of pitch is twice that
of roll. Sethna & Bajaj (1978) predicted further amplitude-modulated motions in
the averaged equations of coupled roll and pitch. Nayfeh h problem several times since then (see, for example, Nayfeh has come back to this problem several times since then (see, for example, Nayfeh 1988; Oh *et al.* 1992). It is interesting to mention that Paulling had approached the averaged equations of coupled roll and pitch. Nayfeh has come back to this
problem several times since then (see, for example, Nayfeh 1988; Oh *et al.* 1992). It
is interesting to mention that Paulling had approached t problem several times since then (see, for example, Nayfeh 1988; Oh *et al.* 1992). It
is interesting to mention that Paulling had approached this problem earlier from a
different angle, investigating whether a ship could different angle, investigating whether a ship could maintain the 'upright' equilibrium position in calm sea when roll is coupled with a prescribed heave or pitch motion (Paulling $\&$ Rosenberg 1959; Paulling 1961). position in calm sea when roll is coupled with a prescribed heave or pitch motion

At that time, it was already known from the works of Grim (1952, 1954) and (Paulling & Rosenberg 1959; Paulling 1961).
At that time, it was already known from the works of Grim (1952, 1954) and
Kerwin (1955) that roll instability could be generated by the restoring becoming
time dependent when a At that time, it was already known from the works of Grim (1952, 1954) and
Kerwin (1955) that roll instability could be generated by the restoring becoming
time dependent when a ship encounters a long regular wave travelli time dependent when a ship encounters a long regular wave travelling in the same direction. Fundamentally, this problem, as well as the problem studied by Paulling, can be reduced to a study of an equation of motion with a direction. Fundamentally, this problem, as well as the problem studied by Paulling, direction. Fundamentally, this problem, as well as the problem studied by Paulling,
can be reduced to a study of an equation of motion with a harmonically varying
stiffness term ('Mathieu' type). These pioneering studies can be reduced to a study of an equation of motion with a harmonically varying
stiffness term ('Mathieu' type). These pioneering studies have inspired significant
research subsequently (see, for example, Blocki 1980; Sanc stiffness term ('Mathieu' type). These pioneering studies have inspired significant
research subsequently (see, for example, Blocki 1980; Sanchez & Nayfeh 1990; Kan
1992). Liaw *et al.* (1992) found chaos in heave-excited research subsequently (see, for example, Blocki 1980; Sanchez & Nayfeh 1990; Kan 1992). Liaw *et al.* (1992) found chaos in heave-excited roll of a barge in head seas. The interest in nonlinear ship dynamics started to su

1992). Liaw *et al.* (1992) found chaos in heave-excited roll of a barge in head seas.
The interest in nonlinear ship dynamics started to surge in the 1970s; but at that time the computers were still at an embryonic stage The interest in nonlinear ship dynamics started to surge in the 1970s; but at that
time the computers were still at an embryonic stage and it was perhaps inevitable that
prominence would be given to analytical methods. Unf prominence would be given to analytical methods. Unfortunately, these methods are not only extremely laborious but they also require that the nonlinearities be weak, thus eliminating much of the most dynamically interesting part of the behaviour.
For the ship-capsize problem in particular, while the non thus eliminating much of the most dynamically interesting part of the behaviour. thus eliminating much of the most dynamically interesting part of the behaviour.
For the ship-capsize problem in particular, while the nonlinearity of damping can
be considered as mild, the nonlinearity of restoring is str For the ship-capsize problem in particular, while the nonlinearity of damping can
be considered as mild, the nonlinearity of restoring is strong, and it is inconsistent
to examine capsize without considering a fully nonlin be considered as mild, the nonlinearity of restoring is strong, and it is incons
to examine capsize without considering a fully nonlinear restoring curve. A dif
viewpoint would thus be needed if an effective solution were to examine capsize without considering a fully nonlinear restoring curve. A different viewpoint would thus be needed if an effective solution were to be achieved.
The vast increase in computer power realized in the 1980s a

viewpoint would thus be needed if an effective solution were to be achieved.
The vast increase in computer power realized in the 1980s and 1990s brought a
wide range of new techniques of numerical analysis of nonlinear dyn The vast increase in computer power realized in the 1980s and 1990s brought a wide range of new techniques of numerical analysis of nonlinear dynamical systems into the limelight. These went well beyond the ordinary simula into the limelight. These went well beyond the ordinary simulation based on direct
integration of the equation of motion. Numerical algorithms were developed for car-
rying out continuation of steady states; for directly l integration of the equation of motion. Numerical algorithms were developed for caridentifying the stable and unstable manifolds either directly or through a vast num-

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ber of automated simulations that unveil the basin of attraction (for a comprehensive
overview see, for example, Foale & Thompson (1991)). Techniques for the characteriber of automated simulations that unveil the basin of attraction (for a comprehensive overview see, for example, Foale & Thompson (1991)). Techniques for the characterization of the responses and also for the extraction o overview see, for example, Foale & Thompson (1991)). Techniques for the characterization of the responses and also for the extraction of possible differentiable dynamics from experimental data series have also been deve zation of the responses and also for the extraction of possible differentiable dynamics tion of the responses and also for the extraction of possible differentiable dynamics
om experimental data series have also been developed.
The technique of steady-state continuation (also known as 'path following') was
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from experimental data series have also been developed.
The technique of steady-state continuation (also known as 'path following') was
applied very quickly to the neighbouring field of flight dynamics (Mehra & Carroll
198 applied very quickly to the neighbouring field of flight dynamics (Mehra $\&$ Carroll 1980).[†] However, another decade would pass before the technique was used in the study of multi-degree ship motions. Continuation is the technique employed in order to determine how a steady motion changes quantitatively as well as qualitatively when some control parameter is varied. Numerical codes of this kind, tracing stationary and periodic states and passing successfully over bif when some control parameter is varied. Numerical codes of this kind, tracing stawhen some control parameter is varied. Numerical codes of this kind, tracing stationary and periodic states and passing successfully over bifurcation points, have been written by a number of people (Keller 1977; Doedel 198 tionary and periodic states and passing successfully over bifurcation points, have
been written by a number of people (Keller 1977; Doedel 1981; Kubicek & Marek
1983; Holodniok & Kubicek 1984; Rheinboldt 1986; Seydel 1988; 1983; Holodnick & Kubicek 1984; Rheinboldt 1986; Seydel 1988; and others). Continuation based on Kubicek's method, coupled with simultaneous stability analysis, was used for investigating the directional stability of ship tinuation based on Kubicek's method, coupled with simultaneous stability analysis, tinuation based on Kubicek's method, coupled with simultaneous stability analysis,
was used for investigating the directional stability of ships with a surge, sway, yaw
and roll mathematical model (Spyrou 1990). Diagrams o was used for investigating the directional stability of ships with a surge, sway, yaw
and roll mathematical model (Spyrou 1990). Diagrams of steering for multi-degree-
of-freedom ship manoeuvring, derived for operation in of-freedom ship manoeuvring, derived for operation in calm conditions and also in time, continuation was employed for the study of some aspects of the behaviour of a ship slowly turning in waves (Falzarano *et al.* 1990). uniform wind, showed the existence of fold and Hopf bifurcations. At about the same

Extensive studies of the bifurcating behaviour of marine vehicles, on the basis of ship slowly turning in waves (Falzarano *et al.* 1990).
Extensive studies of the bifurcating behaviour of marine vehicles, on the basis of simulation or by extracting simple generic models, were carried out at the Univers Extensive studies of the bifurcating behaviour of marine vehicles, on the basis of
simulation or by extracting simple generic models, were carried out at the University
of Michigan in the late 1980s. These studies were foc of Michigan in the late 1980s. These studies were focused on the behaviour of moored tankers (single point initially, and, more recently, multi-line), and they pointed out of Michigan in the late 1980s. These studies were focused on the behaviour of moored
tankers (single point initially, and, more recently, multi-line), and they pointed out
the existence of pitchfork, Hopf and period-doubl tankers (single point initially, and, more recently, multi-line), and they pointed out
the existence of pitchfork, Hopf and period-doubling bifurcations and also the pos-
sibility of chaos (Papoulias & Bernitsas 1988; Chu the existence of pitchfork, Hopf and period-doubling bifurcations and also the pos-
sibility of chaos (Papoulias & Bernitsas 1988; Chung & Bernitsas 1992). A problem
of a similar nature (the behaviour of moored or anchore sibility of chaos (Papoulias & Bernitsas 1988; Chung & Bernitsas 1992). A problem
of a similar nature (the behaviour of moored or anchored tankers) was studied in
Germany (Jiang *et al.* 1987; Sharma *et al.* 1988; Schelli of a similar nature (the behaviour of moored or anchored tankers) was studied in
Germany (Jiang *et al.* 1987; Sharma *et al.* 1988; Schellin *et al.* 1990). Researchers
there carried out stability analyses on the basis o Germany (Jiang *et al.* 1987; Sharma *et al.* 1988; Schellin *et al.* 1990). Researchers there carried out stability analyses on the basis of a quite-advanced surge-sway-
yaw mathematical model that included the so-called there carried out stability analyses on the basis of a quite-advanced surge-sway-
vaw mathematical model that included the so-called memory effect discussed above. Aghamohammadi & Thompson (1990) studied experimentally 'fish-tailing' instabili-
ties of a tanker at a single point mooring. Gottlieb & Yim (1993) predicted instability
and chaos in a multi-point mooring system modelled w Aghamohammadi & Thompson (1990) studied experimentally 'fish-tailing' instabili-
ties of a tanker at a single point mooring. Gottlieb & Yim (1993) predicted instability
and chaos in a multi-point mooring system modelled w ties of a tanker at a single point mooring. Gottlieb & Yim (1993) predicted instability
and chaos in a multi-point mooring system modelled with a simple surge equation
having nonlinear restoring and a coupled wave-structu having nonlinear restoring and a coupled wave-structure exciting force. Choi & Lou
(1993) studied the low drift motion of a tanker induced by the nonlinearity of the having nonlinear restoring and a coupled wave-structure exciting force. Choi & Lou (1993) studied the low drift motion of a tanker induced by the nonlinearity of the mooring line. Jiang (1997) found a Hopf bifurcation cre (1993) studied the low drift motion of a tanker induced by the nonlinearity of the mooring line. Jiang (1997) found a Hopf bifurcation creating yaw oscillations in a tug-tanker tow, depending on the towline length. Contro mooring line. Jiang (1997) found a Hopf bifurcation creating yaw oscillations in a
tug-tanker tow, depending on the towline length. Control studies on the bifurcations
of marine vehicles were carried out by Papoulias (1991 tug-tanker tow, depending on the towline length. Control studies on the bifurcations of marine vehicles were carried out by Papoulias (1991) and Papoulias & Oral (1995) .
In all these years the study of nonlinear rolli

of marine vehicles were carried out by Papoulias (1991) and Papoulias & Oral (1995).
In all these years the study of nonlinear rolling in beam seas continued to be top-
ical. Nayfeh & Khdeir (1986 a, b) and Papanikolaou & In all these years the study of nonlinear rolling in beam seas continued to be top-
ical. Nayfeh & Khdeir (1986 a, b) and Papanikolaou & Zaraphonitis (1987) presented
studies of large-amplitude rolling based on a combinat ical. Nayfeh & Khdeir (1986 a, b) and Papanikolaou & Zaraphonitis (1987) presented
studies of large-amplitude rolling based on a combination of analytical perturbation-
based techniques and digital-analogue simulations. V studies of large-amplitude rolling based on a combination of analytical perturbation-
based techniques and digital–analogue simulations. Virgin (1987) concentrated on the
onset of chaotic roll oscillations occurring throug based techniques and digital-analogue simulations. Virgin (1987) concentrated on the onset of chaotic roll oscillations occurring through a period-doubling cascade, which
he observed on the basis of Poincaré maps. Thompso he observed on the basis of Poincaré maps. Thompson and co-workers (Thompson $\&$ Soliman 1990; Rainey $\&$ Thompson 1991) offered a new perspective on the he observed on the basis of Poincaré maps. Thompson and co-workers (Thompson & Soliman 1990; Rainey & Thompson 1991) offered a new perspective on the ship-capsize problem by considering the capsize process as dynamically e

ip-capsize problem by considering the capsize process as dynamically equivalent

[†] Recent developments in aircraft dynamics are summarized in a Theme Issue of *Philosophical Trans-*
 ions of the Boyal Society of London actions of the Royal Society of London (see Thompson & MacMillen 1998).

Figure 6. Simple analogues for ship dynamics in waves. (a) Beam sea rolling; (b) surging and surf-riding; (c) parametric; (d) pure loss.

to the escape of a ball rolling in a potential well, which is an intrinsically transient to the escape of a ball rolling in a potential well, which is an intrinsically transient
phenomenon (figure 6). One of the first major contributions was the proposal of a
diagram for the practical assessment of a hull's c to the escape of a ball rolling in a potential well, which is an intrinsically transient
phenomenon (figure 6). One of the first major contributions was the proposal of a
diagram for the practical assessment of a hull's c phenomenon (figure 6). One of the first major contributions was the proposal of a
diagram for the practical assessment of a hull's capsizability, which became known
as the *transient capsize diagram* (figure 7). Extensive diagram for the practical assessment of a hull's capsizability, which became known
as the *transient capsize diagram* (figure 7). Extensive cell-mapping and continua-
tion studies were performed for a roll equation with d as the *transient capsize diagram* (figure 7). Extensive cell-mapping and continuation studies were performed for a roll equation with direct or parametric forcing (see, for example, Thompson *et al.* 1992). The efforts to tion studies were performed for a roll equation with direct or parametric forcing
(see, for example, Thompson *et al.* 1992). The efforts to translate the information
about fractal basin boundaries into design criteria ag (see, for example, Thompson *et al.* 1992). The efforts to translate the information
about fractal basin boundaries into design criteria against transient capsize were
very notable. A simple design formula, derived from t very notable. A simple design formula, derived from the displacement magnification of the linear resonance and validated by Melnikov theory and simulation, was put for-
ward. Another significant finding was that the maximum ('sustainable') wave slope
at which capsize is still resisted is very much reduce ward. Another significant finding was that the maximum ('sustainable') wave slope ward. Another significant finding was that the maximum ('sustainable') wave slope
at which capsize is still resisted is very much reduced by the existence of even a small
amount of bias (figure 8). Thus, a stability assess at which capsize is still resisted is very much reduced by the existence of even a small
amount of bias (figure 8). Thus, a stability assessment based on a symmetric ship is
bound to give a dangerous non-conservative capsi bound to give a dangerous non-conservative capsize threshold (for a review of this research see Thompson (1997)). A recent study of the coupled roll and heave revealed a capsize-suppression mechanism introduced by the heave coupling (Thompson $\&$ de Souza 1996). research see Th
a capsize-supp:
Souza 1996).
In the late 1 Exapsize-suppression mechanism introduced by the heave coupling (Thompson & de
uza 1996).
In the late 1980s/early 1990s, capsize due to transient rolling had become a 'hot'
pic. In Japan, Kan (1992) followed a similar lin

In the late 1980s/early 1990s, capsize due to transient rolling had become a 'hot' topic. In Japan, Kan (1992) followed a similar line of research to that of Thompson, with the important addition, however, of extensive model experiments in the

Figure 7. Transient capsize diagram (Rainey & Thompson 1991).

Figure 7. Transient capsize diagram (Rainey & Thompson 1991).

large open square tank of the ship dynamics division of the Ship Research Institute of

Tokyo In the USA Nayfeh & Sanchez (1990) presented numerical safe basi large open square tank of the ship dynamics division of the Ship Research Institute of Tokyo. In the USA, Nayfeh & Sanchez (1990) presented numerical safe basins for the roll motion in beams and in longitudinal waves (San large open square tank of the ship dynamics division of the Ship Research Institute of Tokyo. In the USA, Nayfeh & Sanchez (1990) presented numerical safe basins for the roll motion in beams and in longitudinal waves (Sanc Tokyo. In the USA, Nayfeh & Sanchez (1990) presented numerical safe basins for the roll motion in beams and in longitudinal waves (Sanchez & Nayfeh 1990). Another significant step forward was the use of Melnikov analysis roll motion in beams and in longitudinal waves (Sanchez & Nayfeh 1990). Another
significant step forward was the use of Melnikov analysis for predicting capsizal wave
slopes in beam regular waves (Falzarano *et al.* 1992). significant step forward was the use of Melnikov analysis for predicting capsizal wave
slopes in beam regular waves (Falzarano *et al.* 1992). Use of realistic restoring rep-
resentations, like a fifth- or higher-order po slopes in beam regular waves (Falzarano *et al.* 1992). Use of realistic restoring rep-
resentations, like a fifth- or higher-order polynomial, is, however, problematic when
the analytical route is followed (Scolan 1998). resentations, like a fifth- or higher-order polynomial, is, however, problematic when
the analytical route is followed (Scolan 1998). Bikdash *et al.* (1994) examined the
equivalence between quadratic and cubic damping no the analytical route is followed (Scolan 1998). Bikdash *et al.* (1994) examined the equivalence between quadratic and cubic damping nonlinearities from a Melnikov perspective. Hsieh *et al.* (1994) adapted the Melnikov ap perspective. Hsieh *et al.* (1994) adapted the Melnikov approach for a random exciperspective. Hsieh *et al.* (1994) adapted the Melnikov approach for a random excitation using the concept of Wiggins (1991) for phase flux transport out of the safe basin. This approach was extended for a biased vessel by tation using the concept of Wiggins (1991) for phase flux transport out of the safe
basin. This approach was extended for a biased vessel by Jiang *et al.* (1996). The
interfacing of nonlinear dynamics and stochastic exci interfacing of nonlinear dynamics and stochastic excitation has also been attempted
by others (see, for example, Francescutto 1990).

Liquids inside tanks or a quantity of water shipped on the deck can incur a sigby others (see, for example, Francescutto 1990).
Liquids inside tanks or a quantity of water shipped on the deck can incur a significant effect on the roll dynamics. This problem is a complex one, especially when
impacting Liquids inside tanks or a quantity of water shipped on the deck can incur a significant effect on the roll dynamics. This problem is a complex one, especially when impacting loads due to sloshing can take place, and it ha nificant effect on the roll dynamics. This problem is a complex one, especially when
impacting loads due to sloshing can take place, and it has been tackled using meth-
ods of varying sophistication (for a review of some impacting loads due to sloshing can take place, and it has been tackled using methods of varying sophistication (for a review of some earlier ideas see Caglayan & Storch (1981)). One of the first studies was by Dillingham Storch (1981)). One of the first studies was by Dillingham (1981), where the solution of the deck-flow problem was coupled with the body's roll motion. Recently, Storch (1981)). One of the first studies was by Dillingham (1981), where the solution of the deck-flow problem was coupled with the body's roll motion. Recently, Armenio & Francescutto (1996) followed a similar approach, b tion of the deck-flow problem was coupled with the body's roll motion. Recently,
Armenio & Francescutto (1996) followed a similar approach, but they tackled the
internal fluid-motion problem by solving the Reynolds averag Armenio & Francescutto (1996) followed a similar approach, but they tackled the internal fluid-motion problem by solving the Reynolds averaged Navier-Stokes equations (RANSE). An approach with a different focus was that o internal fluid-motion problem by solving the Reynolds averaged Navier-Stokes equations (RANSE). An approach with a different focus was that of Murashige & Aihara (1998 a, b), who substituted the internal liquid with a lum tions (RANSE). An approach with a different focus was that of Murashige & Aihara (1998 a, b), who substituted the internal liquid with a lumped mass placed at the instantaneous centre of gravity of the liquid, which was f $(1998a, b)$, who substituted the internal liquid with a lumped mass placed at the instantaneous centre of gravity of the liquid, which was further assumed always to have a flat surface. This simplification did not take in instantaneous centre of gravity of the liquid, which was further assumed always
to have a flat surface. This simplification did not take into account sloshing or
hydraulic jump effects, which certainly affect the dynamics; *Phil. Trans. R. Soc. Lond.* A (2000) *Phil. Trans. R. Soc. Lond.* A (2000)

Figure 8. Sensitivity of capsize to bias (Thompson 1997).
this approach revealed a rich content in terms of nonlinear behaviour and also robust
chaos. The authors showed that some nonlinear features could easily be reprodu this approach revealed a rich content in terms of nonlinear behaviour and also robust
chaos. The authors showed that some nonlinear features could easily be reproduced
experimentally in the laboratory chaos. The authors showed that some nonlinear features could easily be reproduced experimentally in the laboratory.

Despite the fact that most of the nonlinear-dynamics research has been inspired by experimentally in the laboratory.
Despite the fact that most of the nonlinear-dynamics research has been inspired by
the capsize problem, it is well known that nonlinear behaviour may also originate in
other motion directi Despite the fact that most of the nonlinear-dynamics research has been inspired by
the capsize problem, it is well known that nonlinear behaviour may also originate in
other motion directions. For example, many ships are other motion directions. For example, many ships are *directionally unstable*, and their steering diagram is S-shaped, tending to turn to port or to starboard depending on the initial condition, even with the rudder undeflected (figure 9). Several ships have experienced a sudden loss of directional control during their operation, a phenomenon known as *broaching*. They are more vulnerable wh experienced a sudden loss of directional control during their operation, a phenomenon experienced a sudden loss of directional control during their operation, a phenomenon
known as *broaching*. They are more vulnerable when approached from the stern by
steep and relatively long waves with celerity near to t known as *broaching*. They are more vulnerable when approached from the stern by
steep and relatively long waves with celerity near to the ship's speed. Broaching is,
before anything else, a yaw stability problem. However, steep and relatively long waves with celerity near to the ship's speed. Broaching is,
before anything else, a yaw stability problem. However, in the course of the tight turn
that follows the 'loss of heading', capsize may before anything else, a yaw stability problem. However, in the course of the tight turn
that follows the 'loss of heading', capsize may be incurred. For a study of this, 'post-
critical', stage of broaching, the combined y that follows the 'loss of heading', capsize may be incurred. For a study of this, 'post-
critical', stage of broaching, the combined yaw-roll dynamics need to be considered.
It seems that Davidson (1948) was the first to critical', stage of broaching, the combined yaw-roll dynamics need to be considered.
It seems that Davidson (1948) was the first to point out that a directionally stable
vessel in calm water could become unstable in follo It seems that Davidson (1948) was the first to point out that a directionally stable
vessel in calm water could become unstable in following waves. Wahab & Swaan
(1964), Eda (1972) and Motora *et al.* (1981) provided furth vessel in calm water could become unstable in following waves. Wahab & Swaan (1964), Eda (1972) and Motora *et al.* (1981) provided further insights. On the basis of linearized equations, they showed that for the 'right w (1964), Eda (1972) and Motora *et al.* (1981) provided further insights. On the basis of linearized equations, they showed that for the 'right wave', instability will occur when the ship lies on the down slope with the st when the ship lies on the down slope with the stern near the crest. Experiments *Phil. Trans. R. Soc. Lond.* A (2000)

of broaching on the basis of free-running models in square basins were pioneered by Nicholson (1974), Fuwa *et al.* (1982) and Marshfield (1987). The application of broaching on the basis of free-running models in square basins were pioneered
by Nicholson (1974), Fuwa *et al.* (1982) and Marshfield (1987). The application
of a nonlinear-dynamics approach recently produced a fundam by Nicholson (1974), Fuwa *et al.* (1982) and Marshfield (1987). The application of a nonlinear-dynamics approach recently produced a fundamental understanding about the phenomena underlying broaching. The key concepts an of a nonlinear-dynam
about the phenomen
summarized in §4.
Surf-riding is anot about the phenomena underlying broaching. The key concepts and developments are summarized in $\S 4$.
Surf-riding is another nonlinear type of behaviour, having its origin in the surge

summarized in $\S 4$.
Surf-riding is another nonlinear type of behaviour, having its origin in the surge
dynamics. It is particularly interesting because it can work as a precursor to broach-
ing. A ship may be forced to a Surf-riding is another nonlinear type of behaviour, having its origin in the surge
dynamics. It is particularly interesting because it can work as a precursor to broach-
ing. A ship may be forced to advance with a speed eq dynamics. It is particularly interesting because it can work as a precursor to broaching. A ship may be forced to advance with a speed equal to the wave celerity, despite the fact that the propeller thrust corresponds to a ing. A ship may be forced to advance with a speed equal to the wave celerity, despite
the fact that the propeller thrust corresponds to a considerably lower, or higher,
speed. Such behaviour was first studied by Grim (1951 speed. Such behaviour was first studied by Grim (1951) , and was reconsidered by him later (Grim 1983), pointing out the analogy with the behaviour of a pendulum under constant torque. Experimental evidence was provided him later (Grim 1983), pointing out the analogy with the behaviour of a pendulum him later (Grim 1983), pointing out the analogy with the behaviour of a pendulum
under constant torque. Experimental evidence was provided by Du Kane & Goodrich
(1962). Kan (1990) investigated the evolution of asymmetric s under constant torque. Experimental evidence was provided by Du Kane & Goodrich (1962). Kan (1990) investigated the evolution of asymmetric surging and the transition to surf-riding when the peak of the fluctuating surge v sition to surf-riding when the peak of the fluctuating surge velocity reaches the wave celerity. Similar studies were undertaken in the same period by Umeda (1990). Surf-riding can trigger broaching when the angle between the direction of the waves wave celerity. Similar studies were undertaken in the same period by Umeda (1990).
Surf-riding can trigger broaching when the angle between the direction of the waves
and the ship is non-zero (quartering waves). In this la Surf-riding can trigger broaching when the angle between the direction of the waves
and the ship is non-zero (quartering waves). In this laterally expanded space, the
surf-riding states belong to a closed curve, of which f and the ship is non-zero (quartering waves). In this laterally expanded space, the
surf-riding states belong to a closed curve, of which fold and Hopf bifurcations are
common features. Chaotic surf-riding based on the Feig surf-riding states belong to a clos
common features. Chaotic surf-ri-
predicted (Spyrou 1995, 1996b).
For a craft moving at a very hipredicted (Spyrou 1995, 1996b).
For a craft moving at a very high speed, some part of the vertical lift force sup-

predicted (Spyrou 1995, 1996*b*).
For a craft moving at a very high speed, some part of the vertical lift force sup-
porting the hull is of a hydrodynamic nature due to the occurrence of *planing*. High-
speed craft in pla For a craft moving at a very high speed, some part of the vertical lift force supporting the hull is of a hydrodynamic nature due to the occurrence of *planing*. High-speed craft in planing conditions are known to exhibit porting the hull is of a hydrodynamic nature due to the occurrence of *planing*. High-
speed craft in planing conditions are known to exhibit a variety of dynamic insta-
bilities. A very well-known case is porpoising, an speed craft in planing conditions are known to exhibit a variety of dynamic instabilities. A very well-known case is porpoising, an instability of the coupled heave and pitch (Martin 1978; Troesch & Falzarano 1992). Its si and pitch (Martin 1978; Troesch & Falzarano 1992). Its simplest manifestation is a self-sustained oscillation in calm sea (implying the occurrence of a Hopf bifurcation event) when the speed exceeds a certain threshold. Other known types of unconventional behaviour are sudden heel, chine walking (roll os self-sustained oscillation in calm sea (implying the occurrence of a Hopf bifurcation
event) when the speed exceeds a certain threshold. Other known types of unconven-
tional behaviour are sudden heel, chine walking (roll event) when the speed exceeds a certain threshold. Other known types of unconventional behaviour are sudden heel, chine walking (roll oscillation), bow diving, and the pitch-yaw-roll oscillations known as 'corkscrew' (Blou tional behaviour are sudden heel, chine walking (roll oscillation), bow diving, and
the pitch-yaw-roll oscillations known as 'corkscrew' (Blount & Codega 1992). Gen-
erally, high speed is believed to affect dynamic stabil the pitch-yaw-roll oscillations known as 'corkscrew' (Blount & Codega 1992). Generally, high speed is believed to affect dynamic stability very considerably, and, with the current emphasis on high-speed maritime transport erally, high speed is believed to affect dynamic stabilit
the current emphasis on high-speed maritime transpeto
to receive considerable attention in the near future. to receive considerable attention in the near future.
5. The instabilities of the stern quartering sea

5. The instabilities of the stern quartering sea
The work on ship stability of Paulling and co-workers at the University of California
at Berkeley although not falling into the domain of poplinear dynamics, has inspired The work on ship stability of Paulling and co-workers at the University of California
at Berkeley, although not falling into the domain of nonlinear dynamics, has inspired
many developments in this field. The experiments a The work on ship stability of Paulling and co-workers at the University of California
at Berkeley, although not falling into the domain of nonlinear dynamics, has inspired
many developments in this field. The experiments a many developments in this field. The experiments at San Francisco Bay (Chow *et al.* 1974) consolidated the idea that a ship may capsize in a following sea environment when any of the three 'fundamental' instability mecha

- (a) Pure loss of stability. Sudden, non-oscillatory capsize due to slow passage from a negative restoring region (around the wave crest).
- (b) Parametric instability. Gradual build-up of rolling due to internal forcing
(b) Parametric instability. Gradual build-up of rolling due to internal forcing
coming from time-dependent (strictly speaking position-depende coming from time-dependent (strictly speaking position-dependent) restoring.
- (c) Frametic Instability. Gradual bulle-up of folling due to internal forcing
coming from time-dependent (strictly speaking position-dependent) restoring.
(c) Broaching. The sudden loss of controllability in steep waves ap the stern. It gives rise to large heel, and, possibly, to capsize during the tight turn
the stern. It gives rise to large heel, and, possibly, to capsize during the tight turn
triggered by the loss of control) Broaching. The sudden loss of the stern. It gives rise to large heating
gered by the loss of control.

Figure 9. Steering diagram under the effect of a varying parameter such as trim.

Figure 10. See opposite for description.

(a) *A* unified approach for 'pure loss' and parametric instability

The qualitative dynamics of pure loss and parametric instability can be represented The qualitative dynamics of pure loss and parametric instability can be represented
by a nonlinear 'Mathieu' equation with some small damping. The characteristic of
pure loss is that the instability is inflicted and the c The qualitative dynamics of pure loss and parametric instability can be represented
by a nonlinear 'Mathieu' equation with some small damping. The characteristic of
pure loss is that the instability is inflicted and the ca by a nonlinear 'Mathieu' equation with some small damping. The characteristic pure loss is that the instability is inflicted and the capsize occurs during a si passage from a crest. The three main factors that determine su pure loss is that the instability is inflicted and the capsize occurs during a single passage from a crest. The three main factors that determine survivability are:
(a) whether the restoring becomes negative in some region

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(b) the magnitude of some initial heel and/or roll velocity as the ship enters into the negative restoring region: the magnitude of some initial **h** the negative restoring region; the negative restoring region;
(c) whether the speed of the ship relative to the wave celerity is sufficiently low
- whether the speed of the ship relative to the wave celerity is sufficiently low that, given the negative restoring and the initial off-balance position, a heel angle finds the time to develop up to dangerous levels. whether the speed of the ship relative to the wave celer
that, given the negative restoring and the initial off-ba
angle finds the time to develop up to dangerous levels.

angle finds the time to develop up to dangerous levels.
Pure loss is an intrinsically transient phenomenon. The parametric instability on the other hand is traditionally examined on the basis of steady-state stability anal Pure loss is an intrinsically transient phenomenon. The parametric instability on the other hand is traditionally examined on the basis of steady-state stability analysis of the trivial upright equilibrium state using as p other hand is traditionally examined on the basis of steady-state stability analysis of the trivial upright equilibrium state using as parameters the frequency ratio and other hand is traditionally examined on the basis of steady-state stability analysis
of the trivial upright equilibrium state using as parameters the frequency ratio and
the wave steepness. In a practical context, however, of the trivial upright equilibrium state using as parameters the frequency ratio and
the wave steepness. In a practical context, however, what is important is whether
capsize-angle levels are reached within a small number capsize-angle levels are reached within a small number of wave-crest encounters. This calls for resetting the focus on the transient dynamics. When the considered number of waves is small, the required amplitude of variation of restoring can be considerably in excess of the corresponding steady-state amplitude, particularly for the principal and the fundamental resonance, which are the most relevant to ships. An approach based on transient dynamics allows for unification of the treatments of pure loss and parametric instability and for developing an assessment on the basis of a single diagram like figure 10 (Spyrou 2000). and parametric instability and for developing an assessment on the basis of a single

Although Mathieu's equation probably `captures' the fundamental dynamics, consideration of extra features—like water shipped on deck, change of damping due Although Mathieu's equation probably 'captures' the fundamental dynamics, consideration of extra features—like water shipped on deck, change of damping due to deck submergence, etc.—would certainly add 'new dimensions' to sideration of extra features—like water shipped on deck, change of damping due
to deck submergence, etc.—would certainly add 'new dimensions' to this analysis.
Another matter of concern is the nature of the excitation: oce to deck submergence, etc.—would certainly add 'new dimensions' to this analysis.
Another matter of concern is the nature of the excitation: ocean waves very rarely
constitute a 'monochromatic sea'. Even in such a highly id Another matter of concern is the nature of the excitation: ocean waves very rarely constitute a 'monochromatic sea'. Even in such a highly idealized environment, the geometry of real ships' hulls could only result in a cyc geometry of real ships' hulls could only result in a cyclic variation of restoring by coincidence. Subsequently, a Hill-type equation would be deemed more appropriate, geometry of real ships' hulls could only result in a cyclic variation of restoring by
coincidence. Subsequently, a Hill-type equation would be deemed more appropriate,
but there is little possibility that some specific for coincidence. Subsequently, a Hill-type equation would be deemed more appropriate,
but there is little possibility that some specific form could be adopted as a generic
model of design excitation. Not only is the excitation but there is little possibility that some specific form could be adopted as a generic model of design excitation. Not only is the excitation non-cyclic, but its main characteristics may be maintained only for limited time. model of design excitation. Not only is the excitation non-cyclic, but its main characteristics may be maintained only for limited time. For this reason, the asymptotic stability information derived from the Strutt diagram acteristics may be maintained only for limited time. For this reason, the asymptotic
stability information derived from the Strutt diagram should be treated with caution.
Viewing these problems from a different perspective stability information derived from the Strutt diagram should be treated with caution.
Viewing these problems from a different perspective, several authors have considered
a stochastically varying parametric term (see, for a stochastically varying parametric term (see, for example, Roberts 1982), aiming to develop some kind of 'statistical' ship-stability criterion.

Coupling with other motions will undoubtedly bring about a number of significant new effects into the dynamics: coupling of roll with lateral and rudder motions should Coupling with other motions will undoubtedly bring about a number of significant
new effects into the dynamics: coupling of roll with lateral and rudder motions should
influence the build-up of roll as the heading of the s from the dynamics: coupling of roll with lateral and rudder motions should
influence the build-up of roll as the heading of the ship will be changing and a sway
force will be excited. Another influence, examined in detail force will be excited. Another influence, examined in detail by Spyrou in this issue (pp. 1813–1834), arises when the ship cannot move with a nearly constant surge velocity due to the relative strength of the longitudinal (pp. $1813-1834$), arises when the ship cannot move with a nearly constant surge.

(*b*) *Recent insights into broaching*

Recent studies of broaching have revealed a rich content in terms of nonlinear dynamics (Spyrou 1996a, c, 1997a). Broaching may occur during the transition

Figure 10. A unifying diagram for capsize due to pure loss and due to parametric instability. The
domain of capsize due to the parametric scenario is based on escape within eight cycles. The white Figure 10. A unifying diagram for capsize due to pure loss and due to parametric instability. The domain of capsize due to the parametric scenario is based on escape within eight cycles. The white regions that evist inside domain of capsize due to the parametric scenario is based on escape within eight cycles. The white regions that exist inside the principal and fundamental resonance regions indicate the occurrence of a 'quick' parametric-t regions that exist inside the principal and fundamental resonance regions indicate the occurrence of a

Figure 11. Overview of the nonlinear dynamics of broaching.

towards surf-riding, or it may occur at a lower speed (and usually with higher waves) towards surf-riding, or it may occur at a lower speed (and usually with higher waves) due to loss of stability of the ordinary periodic yaw motion. The sequence of the phe-
nomena involved in the two routes under gradual i towards surf-riding, or it may occur at a lower speed (and usually with higher waves)
due to loss of stability of the ordinary periodic yaw motion. The sequence of the phe-
nomena involved in the two routes, under gradual nomena involved in the two routes, under gradual increase of the nominal Froude
number, is summarized in figure 11.

The evolution of the qualitative surge dynamics and the onset of surf-riding are number, is summarized in figure 11.
The evolution of the qualitative surge dynamics and the onset of surf-riding are
shown on planes $(a)-(d)$ in figure 11. When the heading of the ship does not coincide
with the wave direct The evolution of the qualitative surge dynamics and the onset of surf-riding are
shown on planes $(a)-(d)$ in figure 11. When the heading of the ship does not coincide
with the wave direction, the surf-riding equilibria belo shown on planes $(a)-(d)$ in figure 11. When the heading of the ship does not coincide
with the wave direction, the surf-riding equilibria belong to a closed curve having
unstable (in surge) points near the crest and stable with the wave direction, the surf-riding equilibria belong to a closed curve having unstable (in surge) points near the crest and stable or unstable points (depending on the proportional gain of the autopilot) near the tr on the proportional gain of the autopilot) near the trough (plane (e)). When a ship on the proportional gain of the autopilot) near the trough (plane (e)). When a ship
operates with a non-zero heading relative to the wave, and the homoclinic connec-
tion event (see planes (e) and (d)) destroys the per operates with a non-zero heading relative to the wave, and the homoclinic connection event (see planes (c) and (d)) destroys the periodic response, the remaining possible motions are either surf-riding or a rapid turnin possible motions are either surf-riding or a rapid turning motion that corresponds to broaching. Which of the two will occur depends on whether or not the autopilot gain is sufficient for attracting the orbit leaving the periodic pattern, and, thus, creating capture into stable surf-riding near the trough. An example of broaching is presented on plane (f) . It was discovered that creating capture into stable surf-riding near the trough. An example of broaching is creating capture into stable surf-riding near the trough. An example of broaching is
presented on plane (f). It was discovered that surf-riding could be realized in a peri-
odic sense (Hopf bifurcation) and even in a chao presented on plane (f). It was discovered that surf-riding could be realized in a periodic sense (Hopf bifurcation) and even in a chaotic sense (period-doubling cascade).
On planes $(g)-(i)$ the key phenomena can be seen alo On planes $(g)-(i)$ the key phenomena can be seen along with their sequence when the angle of the rudder, δ , is treated as the control variable (Spyrou 1996b). is planes $(g)-(i)$ the key phenomena can be seen along with their sequence when
e angle of the rudder, δ , is treated as the control variable (Spyrou 1996b).
Finally, we describe the occurrence of broaching directly from

the angle of the rudder, δ , is treated as the control variable (Spyrou 1996b).
Finally, we describe the occurrence of broaching directly from the periodic pattern
and without serious involvement of the surge dynamics (Finally, we describe the occurrence of broaching directly from the periodic pattern
and without serious involvement of the surge dynamics (plane (j)). At a critical
heading (for a certain ship and with fixed wave charact and without serious involvement of the surge dynamics (plane (j)). At a critical heading (for a certain ship and with fixed wave characteristics), a flip bifurcation occurs, creating a stable subharmonic response. This c *Phil. Trans. R. Soc. Lond.* A (2000)

autopilot: $(3,3,1)$, GM = 1.51 m

Figure 12. 'Multiple-effect' global analysis targeting the process of escape from surf-riding. The layout of the broaching domain and the domain of cansize eroding the broaching domain are Figure 12. 'Multiple-effect' global analysis targeting the process of escape from surf-riding. The layout of the broaching domain and the domain of capsize eroding the broaching domain are shown (Spyrou 1997b) layout of the broaching domain and the domain of capsize eroding the broaching domain are shown (Spyrou 1997b).

amplitude of yaw oscillation, leading, shortly, to a backwards turn of the response curve, which precipitates a sudden and dangerous jump to resonance. The ensuing transient behaviour will correspond to cumulative-type broaching (Spyrou 1997a).

The transient dynamics of broaching have been studied thus far in respect of two transient behaviour will correspond to cumulative-type broaching (Spyrou 1997a).
The transient dynamics of broaching have been studied thus far in respect of two
specific transitions. The first transition referred to the The transient dynamics of broaching have been studied thus far in respect of two
specific transitions. The first transition referred to the process of escape from surf-
riding after voluntary reduction of engine power or specific transitions. The first transition referred to the process of escape from surf-
riding after voluntary reduction of engine power or change of heading (see figure 12
and Spyrou (1996c)). A second scenario considere riding after voluntary reduction of engine power or change of heading (see figure 12 and Spyrou (1996*c*)). A second scenario considered targeted the disappearance of the periodic motion due to the homoclinic connection b

6. Future directions for research

6. Future directions for research
The field of nonlinear ship dynamics is only now approaching maturity, and it is
believed that several exciting new developments will be realized in the near future The field of nonlinear ship dynamics is only now approaching maturity, and it is believed that several exciting new developments will be realized in the near future.
In the authors' opinion, some of the areas in which furt The field of nonlinear ship dynamics is only now approaching maturity, and it is
believed that several exciting new developments will be realized in the near future.
In the authors' opinion, some of the areas in which furt believed that several exciting new developments will be realized in the near future.
In the authors' opinion, some of the areas in which further activity is expected, or would be very welcome, are the following.

(1) Integration of the probabilistic character of the seaway into the study of non-
linear dynamics Integration of the
linear dynamics. *Phil. Trans. R. Soc. Lond.* A (2000)

- (2) More rational description of hull loads taking better account of the detailed shape of a ship hull. More rational descrips
shape of a ship hull. (3) Development of mathematical models of coupled motions.
- (4) Instabilities that are intrinsic to high-speed operation.
-
- (4) Instabilities that are intrinsic to high-speed operation.
(5) Development of improved techniques for analysing multi-degree dynamical systems. (6) Use of the concepts of nonlinear dynamics in the modelling process.
- (6) Use of the concepts of nonlinear dynamics in the modelling (7) Making the link between nonlinear dynamics and design.
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References

- **Aghamohammadi, F. & Thompson, J. M. T. 1990 An experimental study of the large amplitude**

fish-tailing instabilities of a tanker at a single point mooring *Annl. Ocean Res* 12, 25–53 sh-tailing instabilities of a tanker at a single point mooring. *Appl. Ocean Res.* 12, 25–53.

monic V & Francescutte, A, 1996 On the rell motion of a ship with partially filled unbaffed fish-tailinginstabilities of a tanker at a single point mooring. Appl. Ocean Res. 12, 25–53.
Armenio, V. & Francescutto, A. 1996 On the roll motion of a ship with partially filled unbaffled
- fish-tailing instabilities of a tanker at a single point mooring. Appl. Ocean Res. 12, 25–53.
menio, V. & Francescutto, A. 1996 On the roll motion of a ship with partially filled unbaffled
and baffled tanks. Part 1. Mathem menio, V. & Frances
and baffled tanks. Pa
Engng **6**, 278–282.
umann. H. 1055 Boll Baumann, H. 1955 Rollzustande grosser Amplitude in Seitlicher Dunung. *Schiffstechnik*, 4, 189–
- 199. Baumann, H. 1955 Rollzustande grosser Amplitude in Seitlicher Dunung. *Schiffstechnik*, 4, 189–
199.
Beck, R. 1996 Application of modern numerical methods in marine hydrodynamics. *Trans.*
 $SNAME$ 104–519–537
- 199.
ck, R. 1996 Application
SNAME 104, 519–537.
rg⁶ P. Pomeou V. *k*, Vi Berg¶e, P., Pomeau, Y. & Vidal, C. 1984 *Order within chaos*. Wiley.
-
- Bikdash, M., Balachandran, B. & Nayfeh, A. 1994 Melnikov analysis for a ship with a general roll-damping model. *Nonlinear Dyn.* 6, 101-124.
- Blagoveshchensky, S. N. 1962 *Theory of ship motions*. New York: Dover.
- roll-damping model. *Nontinear Dyn.* 6, 101–124.
Blagoveshchensky, S. N. 1962 Theory of ship motions. New York: Dover.
Blocki, W. 1980 Ship safety in connection with parametric resonance of the roll. *Int. Shipbuilding*
Pr agoveshchensky, S.
₂ ocki, W. 1980 Ship s
Progr. **27**, 36–53.
2 unt. D. J. & Code
- Progr. 27, 36–53.
Blount, D. L. & Codega, L. T. 1992 Dynamic stability of planing boats. *Marine Technol*. 29, 4–12.
- Caglayan, I. & Storch, R. L. 1981 Stability of fishing vessels with water on deck: a review. *[J.](http://pippo.ingentaselect.com/nw=1/rpsv/cgi-bin/linker?ext=a&reqidx=/0022-4502^28^2926L.106[aid=540347,csa=0022-4502^26vol=26^26iss=2^26firstpage=106]) Ship Res.* **26**, 106-116. Caglayan,I. & Storch, R. L. 1981 Stability of fishing vessels with water on deck: a review. J.

Ship Res. 26, 106–116.

Cardo, A., Francescutto, A. & Nabergoj, R. 1981 Ultraharmonics and subharmonics in the

rolling moti
- Ship Res. 26, 106–116.

rdo, A., Francescutto, A. & Nabergoj, R. 1981 Ultraharr

rolling motion of a ship. *Int. Shipbuilding Progr.* 28, 326.

198¹ F. J. C. J. V. K. 1993 Nonlinear mogring line Cardo, A., Francescutto, A. & Nabergoj, K. 1981 Ultraharmonics and subharmonics in the
rolling motion of a ship. *Int. Shipbuilding Progr.* **28**, 326.
Choi, H. S. & Lou, J. Y. K. 1993 Nonlinear mooring line induced slow d
- rolling motion of a ship. *Int. Shipbuilding*
ioi, H. S. & Lou, J. Y. K. 1993 Nonline
ALP-tanker. *Ocean Engng* 20, 233–246.
Cow, S. J. Ooklov, O. H. Poulling, J. P. Choi, H. S. & Lou, J. Y. K. 1993 Nonlinear mooring line induced slow drift motion of an
ALP-tanker. Ocean Engng 20, 233–246.
Chow, S. J., Oakley, O. H., Paulling, J. R., Van Slyke, R., Wood, P. D. & Zink, P. F. 1974
Ship m
- ALP-tanker. *Ocean Engng* 20, 233–246.
low, S. J., Oakley, O. H., Paulling, J. R., Van Slyke, R., Wood, P. D. & Zink, P. F. 1974
Ship motions and capsizing in astern seas. Department of Transportation, US Coast Guard,
Wash Ship motions and capsizing in astern seas. Department of Transportation, US Coast Guard, Washington DC, final report. Ship motions and capsizing in astern seas. Department of Transportation, US Coast Guard,
Washington DC, final report.
Chung, W. & Bernitsas, M. 1992 Dynamics of two-line ship towing/mooring systems: bifurca-
tions singula
- Washington DC, final report.
ung, W. & Bernitsas, M. 1992 Dynamics of two-line ship towing/mooring sy
tions, singularities of stability boundaries, chaos. *J. Ship Res.* 36, 123–140.
videon, K. S. M. 1948. A note on the st
- tions,singularities of stability boundaries, chaos. *J. Ship Res.* **36**, 123–140.
Davidson, K. S. M. 1948 A note on the steering of ships in following seas. In *Proc. 7th Int.*
Congress of Applied Mechanics, London. *Congress of Applied Mechanics, Chaos. J. Ship Res.* **36**, 123–140.

Davidson, K. S. M. 1948 A note on the steering of ships in following seas. In *Proc. 7th Int.*
 Congress of Applied Mechanics, London.

Dillingham, J.
-
- Congress of Appuea Mechanics, London.
Dillingham, J. 1981 Motion studies of a vessel with water on deck. *Marine Technol*. 18, 38–50.
Doedel, E. J. 1981 AUTO: a program for the automatic bifurcation analysis of autonomous
 llingham, J. 1981 Motion studies of a
edel, E. J. 1981 AUTO: a program
systems. *Cong. Num.* **30**, 265–272.
L'Enne B^{et} Coodrich, J. B. 1969.7 Doedel, E. J. 1981 AUTO: a program for the automatic bifurcation analysis of autonomous systems. *Cong. Num.* **30**, 265–272.
Du Kane, P. & Goodrich, J. R. 1962 The following sea, broaching and surging. *Trans. RINA*
104–
- systems. Cong.
1 Kane, P. & Go
104, 109–140. *Phil. Trans. R. Soc. Lond.* A (2000)

Eda, H. 1972 Directional stability and control of ships in waves. *J. Ship Res.* 16, 205-218.

- Falzarano, J. M., Stiendtl, A., Troesch, A. & Troger, H. 1990 Bifurcationanalysisofavessel slowly turning in waves. In *Proc. 4th Int. Conference on Stability of Ships and Ocean Vehicles, Naples, Italy*. Naples: Department of Naval Engineering, University of Federico II.
- Falzarano, J. M., Shaw, S. W. & Troesch, A. W. 1992 Application of global methods for analysing *Naples, Italy.* Naples: Department of Naval Engineering, University of Federico II.
Izarano, J. M., Shaw, S. W. & Troesch, A. W. 1992 Application of global methods for analy
dynamical systems to ship rolling and capsizing
- Falzarano, J. M., Shaw, S. W. & Troesch, A. W. 1992 Application of global methods for analysing
dynamical systems to ship rolling and capsizing. *Int. J. Bifurcation Chaos* 2, 101–116.
Foale, S. & Thompson, J. M. T. 1991 dynamical systems to ship rolling and capsizing. *Int. J. Bifurcation C* ale, S. & Thompson, J. M. T. 1991 Geometrical concepts and comp
nonlinear dynamics. *Comp. Meth. Appl. Mech. Engng* 89, 381–394.
ancescutte, A. 1990 Foale,S. & Thompson, J. M. T. 1991 Geometrical concepts and computational techniques of nonlinear dynamics. Comp. Meth. Appl. Mech. Engng 89, 381–394.
Francescutto, A. 1990 On the probability of large-amplitude rolling an
- nonlinear dynamics. *Comp. Meth. Appl. Mech. Engng* 89, 381–394.
ancescutto, A. 1990 On the probability of large-amplitude rolling and capsizing as a consequence of bifurcations. In *Proc. Symp. Dynamics of Marine Vehicles* ancescutto, A. 1990 On the problem

quence of bifurcations. In *Proc. Sy*
 London, pp. 291–304. Elsevier.

ancescutto. A. *kr* Contento G. 199
- London, pp. 291–304. Elsevier.
Francescutto, A. & Contento, G. 1998 The modeling of the excitation of large amplitude rolling
in beam waves. In *Proc. 4th Int. Ship Stability Workshop, Newfoundland, Canada*. *London*, pp. 291–304. Elsevier.
Francescutto, A. & Contento, G. 1998 The modeling of the excitation of large amplitude rolling
in beam waves. In *Proc. 4th Int. Ship Stability Workshop, Newfoundland, Canada.*
Froude, W. F
-
- in beam waves. In Proc. 4th Int. Ship Stability Workshop, Newfoundland, Canada.
Froude, W. F. 1863 Remarks on Mr. Scott Russell's paper on rolling. Trans. INA 3, 232–275.
Fuwa, T., Sugai, K., Yoshino, T. & Yamamoto, T. 198 *of a small high-speed boat*. Papers of the Ship Research Institute, no. 66. Tokyo: Ship Research Institute.
- Gottlieb, O. & Yim, S. C. S. 1993 Drag induced instabilities and chaos in mooring systems. *Ocean Engng* 20, 569-599.
- Grim, O. 1951 Das Schiff in vor actern auflaufender See. *Jahrbuch STG* 45, 264-287.
- Grim, O. 1951 Das Schiff in vor actern auflaufender See. Jahrbuch STG 45, 264–287.
Grim, O. 1952 Rollschwingungen, Stabilität und Sicherheit im Seegang. *Schiffstechnik* 1, 10–21.
Grim, O. 1954 Zur Stabilität der periodisc
- Grim, O. 1951 Das Schiff in Vor actern aunauiender See. Jahrbuch 51 G 43, 204–287.
Grim, O. 1952 Rollschwingungen, Stabilität und Sicherheit im Seegang. Schiffstechnik 1, 10–21.
Grim, O. 1954 Zur Stabilität der periodische *Grim, O. 1954 Zur Stabilität der periodischen, erzwungenen Rollshwingungen eines Schiffes.
Ingenieur-archiv* 22, 55–59.
- Grim, O. 1983 Das Schiff in von achtern kommendem Seegang. *Schiffstechnik* 30, 84–94.
- Ingenieur-archiv 22, 55–59.
Grim, O. 1983 Das Schiff in von achtern kommendem Seegang. *Schiffstechnik* 30, 84–94.
Guckenheimer, J. & Holmes, P. J. 1983 *Nonlinear oscillations, dynamical systems and bifurca-*
tions of vec *tim, O. 1983 Das Schiff in von ac*
tions of vector fields. Springer.
tions of vector fields. Springer.
algebraid: M. & Kubicel: M. 198 tions of vector fields. Springer.
Holodniok, M. & Kubicek, M. 1984 DERPER—an algorithm for the continuation of periodic
- solutions in ordinary differential equations. *J. Comput. Phys.* 55, 254-262. Holodnick, M. & Kubicek, M. 1984 DERPER—an algorithm for the continuation of periodic
solutions in ordinary differential equations. J. Comput. Phys. 55, 254–262.
Hsieh, S., Troesch, A. W. & Shaw, S. W. 1994 A nonlinear pr
- versions in ordinary differential equations. *J. Comput. Phys.* 55, 254–262.
ieh, S., Troesch, A. W. & Shaw, S. W. 1994 A nonlinear probabilistic method
vessel capsizing in random beam seas. *Proc. R. Soc. Lond.* A 446, 19 Hsieh, S., Troesch, A. W. & Shaw, S. W. 1994 A nonlinear probabilistic method for predicting
vessel capsizing in random beam seas. *Proc. R. Soc. Lond.* A 446, 195–211.
Hsu, C. S. 1987 *Cell-to-cell mapping: a method of gl*
- vessel capsizing in random beam seas. Proc. R. Soc. Lond. A 446, 195–211.
Hsu, C. S. 1987 Cell-to-cell mapping: a method of global analysis for nonlinear systems.
Huang, Y. & Sclavounos, P. 1998 Nonlinear ship motions. *J.*
- Huang, Y. & Sclavounos, P. 1998 Nonlinear ship motions. *J. Ship Res.* 42, 120–131.
Hutchison, B. 1990 Seakeeping studies: a status report. *Trans. SNAME* 98, 263–317.
-
- Huang, Y. & Sciavounos, P. 1998 Noninear ship motions. *J. Ship Res.* 42, 120–131.
Hutchison, B. 1990 Seakeeping studies: a status report. *Trans. SNAME* 98, 263–317.
Jiang, C., Troesch, A. W. & Shaw, S. W. 1996 Highly no itchison, B. 1990 Seakeeping studies: a status report of the Shaw, S. W. 1996 High
in random beam seas. *J. Ship Res.* 40, 125–135.
ppg T. 1997 Autonomous cosillations and bifurcations. inrandom beam seas. *J. Ship Res.* 40, 125–135.
Jiang, T. 1997 Autonomous oscillations and bifurcations of a tug-tanker tow. *Ship Technol. Res.*
- *Schiffstechnik* 44, 4-12.
- Jiang, T., Schellin, T. E. & Sharma, S. D. 1987 Manoeuvring simulation of a tanker moored in Schiffstechnik 44, 4–12.

ung, T., Schellin, T. E. & Sharma, S. D. 1987 Manoeuvring simulation of a tanker moored in

steady current including hydrodynamic memory effects and stability analysis. In *Proc. Int.*

Cont. Shin *Conf. Ship Manoeuvrability: Prediction and Achievement*. London: RINA. steady current including hydrodynamic memory effects and stability analysis. In *Proc. Int.*
Conf. Ship Manoeuvrability: Prediction and Achievement. London: RINA.
Kan, M. 1990 *Surging of large amplitude and surf-riding of*
- Conf. Ship Manoeuvrability: Prediction and Achievement. London: RINA.

un, M. 1990 Surging of large amplitude and surf-riding of ships in following seas. Selected

papers in Naval Architecture and Ocean Engineering, no. 28 papers in Naval Architecture and Ocean Engineering, no. 28. Tokyo: Society of Naval Architects of Japan. papers in Naval Architecture and Ocean Engineering, no. 28. Tokyo: Society of Naval Architects of Japan.
Kan, M. 1992 Chaotic capsizing. In *Proc. 20th ITTC Seakeeping Committee and Kansai Fluid-*
Dunamics Research Group,
- **Eacts of Japan.**
 Dynamics Research Group, Osaka Meeting on Seakeeping Committee and Kansai.
 Dynamics Research Group, Osaka Meeting on Seakeeping Performance, pp. 155–180.

² ^D ¹⁰⁷⁷ Numerical solution of bifurc Kan, M. 1992 Chaotic capsizing. In *Proc. 20th ITTC Seakeeping Committee and Kansai Fluid-*
Dynamics Research Group, Osaka Meeting on Seakeeping Performance, pp. 155–180.
Keller, H. B. 1977 Numerical solution of bifurcatio
- *Dynamics Research Group, Osaka Meeting on Seakeeping Performance*

iller, H. B. 1977 Numerical solution of bifurcation and nonlinear eig
 Applications of bifurcation theory (ed. P. H. Rabinowitz). Academic.

www. J. F. Keller, H. B. 1977 Numerical solution of bifurcation and nonlinear eigenvalue problems. In

Applications of bifurcation theory (ed. P. H. Rabinowitz). Academic.

Kerwin, J. E. 1955 Notes on rolling in longitudinal waves. I
-
- Applications of bifurcation theory (ed. P. H. Rabinowitz). Academic.
Kerwin, J. E. 1955 Notes on rolling in longitudinal waves. *Int. Shipbuilding Progr.* 2, 597–614.
Kubicek, M. & Marek, M. 1983 *Computational methods in* rwin, J. E. 1955 Notes
ibicek, M. & Marek, l
structures. Springer. *Phil. Trans. R. Soc. Lond.* A (2000)
- Kuo, C. & Odabashi, A. Y. 1975 Application of dynamic systems approach to ship and ocean vehicle stability. In *Proc. 1st Int. Conf. on Stability of Ships and Ocean Vehicles, University*
of *Strathclyde Glasgow For Strathclyde, Glasgow.* Liam, C. *Y.* 1975 Application of dynamic systems approach to ship and ocean vehicle stability. In *Proc. 1st Int. Conf. on Stability of Ships and Ocean Vehicles, University* of *Strathclyde, Gl*
- of Strathclyde, Glasgow.
ww, C. Y., Bishop, S. R. & Thompson, J. M. T. 1992 Heave-excited rolling motion of a
rectangular vessel in head seas. In *Proc. 2nd Int. Offshore and Polar Engineering Conf., San*
Francisco. June 1 *Francisco, June 1992, vol. III, pp. 615–622.*
Francisco, June 1992, vol. III, pp. 615–622.
Francisco, June 1992, vol. III, pp. 615–622. rectangular vessel in head seas. In Proc. 2nd Int. Offshore and Polar Engineering Conf., San
Francisco, June 1992, vol. III, pp. 615–622.
Marshfield, W. B. 1978 AMTE–NMI capsize experiments. Admiralty Research Establishmen
- Francisco, June 1992, vol. III, pp. 615–62;
arshfield, W. B. 1978 AMTE–NMI capsize
report TM78011. Haslar Gosport Hants.
arshfield, W. B. 1987 Haslar capsize exper report TM78011. Haslar Gosport Hants.
Marshfield, W. B. 1987 Haslar capsize experiments 1977 to 1986. Admiralty Research Estab-
- lishment, report ARE TR87315. Haslar Gosport Hants. Marshfield, W. B. 1987 Haslar capsize experiments 1977 to 1986. Admiralty Research Establishment, report ARE TR87315. Haslar Gosport Hants.
Martin, M. 1978 Theoretical determination of porpoising instability of high speed
- *Ishment, report ARE TF*
J. Ship Res. 22, 32–53.
J. Ship Res. 22, 32–53. Martin, M. 1978 Theoretical determination of porpoising instability of high speed planing boats.
 J. Ship Res. 22, 32–53.

Mehra, H. R. A. & Carroll, J. V. 1980 Bifurcation analysis of aircraft high-angle-of-attack fligh
- J. *Ship Res.* 22, 32–53.

ehra, H. R. A. & Carroll, J. V. 1980 Bifurcation analysis of aircraft high-angle-of-attack flight

dynamics. In *Proc. New Approaches to Nonlinear Problems in Dynamics, SIAM, Philadelphia*

(ed. dynamics. In *Proc. New Approaches to Nonlinear Problems in Dynamics, SIAM, Philadelphia* (ed. P. J. Holmes), pp. 127–146.
- Moon, F. C. (ed.) 1999 *New applications of nonlinear and chaotic dynamics in mechanics*. Dordrecht: Kluwer. Moon, F. C. (ed.) 1999 *New applications of nonlinear and chaotic dynamics in mechanics*.

Dordrecht: Kluwer.

Motora, S., Fujino, M., Koyonagi, M., Ishida, S., Shimada, K. & Maki, T. 1981 *A considera-*
 tion on the mech
- Dordrecht: Kluwer.
ptora, S., Fujino, M., Koyonagi, M., Ishida, S., Shimada, K. & Maki, T. 1981 *A consideration on the mechanism of occurrence of broaching-to phenomena*. Selected Papers in Naval
Architecture and Ocean En tion on the mechanism of occurrence of broaching-to phenomena. Selected Papers in Naval Architecture and Ocean Engineering, no. 150. Tokyo: Society of Naval Architects of Japan. tion on the mechanism of occurrence of broaching-to phenomena. Selected Papers in Naval
Architecture and Ocean Engineering, no. 150. Tokyo: Society of Naval Architects of Japan.
Murashige, S. & Aihara, K. 1998a Coexistence
- Architecture and Ocean Engineering, no. 150. Tokyo
trashige, S. & Aihara, K. 1998a Coexistence of periodi
flooded ship. *Int. J. Bifurcation Chaos* 8, 619–626.
trashige S. & Aihara, K. 1998b Experimental study
- flooded ship. *Int. J. Bifurcation Chaos* 8, 619–626.
Murashige, S. & Aihara, K. 1998b Experimental study of chaotic motion of a flooded ship in waves. *Proc. R. Soc. Lond.* A 454, 2537–2553.
- Nayfeh, A. H. 1988 Undesirable roll characteristics of ships in regular waves. *[J. Ship Res.](http://pippo.ingentaselect.com/nw=1/rpsv/cgi-bin/linker?ext=a&reqidx=/0022-4502^28^2932L.92[aid=540361,csa=0022-4502^26vol=32^26iss=2^26firstpage=92])* **32**, 92–100. Nayfeh,A. H. 1988 Undesirable roll characteristics of ships in regular waves. *J. Ship Res.* 32,
92–100.
Nayfeh, A. H. & Khdeir, A. A. 1986a Nonlinear rolling of ships in regular beam seas. *Int.*
Shiphuilding Progr. 33,
- 92–100.
*y*feh, A. H. & Khdeir, A. A. 1
Shipbuilding Progr. **33**, 40–49.
yfeh A. H. & Khdeir, A. A. 1980 Nayfeh, A. H. & Khdeir, A. A. 1986*a* Nonlinear rolling of ships in regular beam seas. *Int.*

Shipbuilding Progr. 33, 40–49.

Nayfeh, A. H. & Khdeir, A. A. 1986b Nonlinear rolling of biased ships in regular beam seas. *In*
- *Shipbuilding Progr.* **33**, 40–49.
 Shipbuilding Progr. **33**, 89–93.
 Shipbuilding Progr. **33**, 89–93.
 *M*_B *M*_B *M*_B *Sanchoz N*_B *T* Nayfeh, A. H. & Khdeir, A. A. 1986b Nonlinear rolling of biased ships in regular beam seas. *Int.*

Shipbuilding Progr. 33, 89–93.

Nayfeh, A. H. & Sanchez, N. E. 1990 Stability and complicated rolling responses of ships i
- Shipbuilding Progr. **33**, 89–93.

yfeh, A. H. & Sanchez, N. E. 1990 Stability and complic

regular beam seas. *Int. Shipbuilding Progr.* **37**, 331–352.

yfeh A. H. Mook, D. T. & Marshall J. B. 1973 Nonlines Nayfeh, A. H. & Sanchez, N. E. 1990 Stability and complicated rolling responses of ships in regular beam seas. *Int. Shipbuilding Progr.* **37**, 331–352.
Nayfeh, A. H., Mook, D. T. & Marshall, L. R. 1973 Nonlinear coupling
- regular beam seas. *Int. Shipbuilding Progr.* 37,
yfeh, A. H., Mook, D. T. & Marshall, L. R. 19
in ship motions. *J. Hydronautics* 7, 145–152.
cholson, K. 1974 Some parametric model expe
- in ship motions. *J. Hydronautics* **7**, 145–152.
Nicholson, K. 1974 Some parametric model experiments to investigate broaching-to. In *Proc.*
Int. Symp. on the Dynamics of Marine Vehicles and Structures in Waves, London. Int. Symp. on the Dynamics of Marine Vehicles and Structures in Waves, London.
Int. Symp. on the Dynamics of Marine Vehicles and Structures in Waves, London.
Odabashi, A. Y. 1973 Methods of analysing nonlinear ship osc
- Int. Symp. on the Dynamics of Marine Vehicles and Structures in Waves, London.

Iabashi, A. Y. 1973 Methods of analysing nonlinear ship oscillations and stability. University of

Strathclyde, Department of Shipbuilding an Strathclyde, Department of Shipbuilding and Naval Architecture, internal report, no. 08/73.
Odabashi, A. Y. 1977 Ultimate stability of ships. *Trans. RINA* 119, 237–263.
-
- Strathclyde, Department of Shipbuilding and Naval Architecture, internal report, no. 08/73.
Odabashi, A. Y. 1977 Ultimate stability of ships. *Trans. RINA* 119, 237–263.
Odabashi, A. Y. 1978 Conceptual understanding of the labashi, A.
labashi, A.
25, 1–18.
labashi. A Odabashi, A. Y. 1982 A morphology of mathematical stability theory and its application to
- 25, 1–18.
labashi, A. Y. 1982 A morphology of mathematical stability theory and its application to
intact ship stability assessment. In *Proc. 2nd Int. Conf. on Stability of Ships and Ocean*
Vehicles pp. 47–64. Tokyo: Soci Iabashi, A. Y. 1982 A morphology of mathematical stability theometrical stability sases in the *Vehicles*, pp. 47-64. Tokyo: Society of Naval Architects of Japan.
Vehicles, pp. 47-64. Tokyo: Society of Naval Architects o intact ship stability assessment. In Proc. 2nd Int. Conf. on Stability of Ships and Ocean
Vehicles, pp. 47–64. Tokyo: Society of Naval Architects of Japan.
Oh, I., Nayfeh, A. & Mook, D. 1992 Theoretical and experimental s
- Vehicles, pp. 47–64. Tokyo: Society of Naval Architects of Japan.

1, I., Nayfeh, A. & Mook, D. 1992 Theoretical and experimental study of the nonlinearly

coupled heave pitch and roll motions of a ship in longitudinal wav *Naval Hydrodynamics, Seoul, Korea, pp. 93–111.*
Naval Hydrodynamics, Seoul, Korea, pp. 93–111.
Naval Hydrodynamics, Seoul, Korea, pp. 93–111. coupled heave pitch and roll motions of a ship in longitudinal waves. In Proc. 9th Symp. on
Naval Hydrodynamics, Seoul, Korea, pp. 93–111.
Papanikolaou, A. & Zaraphonitis, G. 1987 Computer-aided simulations of large amplit
- Naval Hydrodynamics, Seoul, Korea, pp. 93–111.
panikolaou, A. & Zaraphonitis, G. 1987 Computer-aided simulations of large amplitude remotions of ships in waves and of dynamic stability. *Int. Shipbuilding Progr.* **34**, 198 motions of ships in waves and of dynamic stability. *Int. Shipbuilding Progr.* **34**, 198–206.
- Papoulias, F. A. 1991 Bifurcation analysis of line of sight vehicle guidance using sliding modes.
Int. J. Bifurcation Chaos 1, 845–861.
- The nontinear aynamics of ship motions
Papoulias, F. & Bernitsas, M. 1988 Autonomous oscillations, bifurcations and chaotic response
of moored vessels J. Shin Res. 32, 220–228 poulias, F. & Bernitsas, M. 1988 Autonomous
of moored vessels. *J. Ship Res.* **32**, 220–228.
pouliss. F. A. & Oral. Z. O. 1995 Horf bifurce
- Papoulias,F. & Derlitsas, M. 1988 Attonomous oscillations, bifurcations and chaotic response
of moored vessels. J. Ship Res. 32, 220–228.
Papoulias, F. A. & Oral, Z. O. 1995 Hopf bifurcations and nonlinear studies of gai poulias, F. A. & Oral, Z. O. 1995 Hopf bifurcations and nonline path control of marine vehicles. *Appl. Ocean Res.* 17, 21–32.

ulling L. B. 1961 The transverse stability of a ship in a length
- pathcontrol of marine vehicles. *Appl. Ocean Res.* 17, 21–32.
Paulling, J. R. 1961 The transverse stability of a ship in a longitudinal seaway. *J. Ship Res.* 4, 37–49.
- Pauling, J. R. 1961 The transverse stability or a ship in a longitudinal seaway. J. Ship Res. 4, 37–49.
Paulling, J. R. & Rosenberg, R. M. 1959 On unstable ship motions resulting from nonlinear coupling J. Ship Res. 2, 36 37–49.
ulling, J. R. & Rosenberg, R. M.
coupling. *J. Ship Res.* **2**, 36–46.
uton Jones. J. C. & Conceye, L. 19. Pauling, J. K. & Rosenberg, K. M. 1999 On unstable sinp motions resulting from nonlinear
coupling. J. Ship Res. 2, 36–46.
Peyton Jones, J. C. & Cancaya, I. 1997 A note on the computation of maximum roll amplitudes
in regu
- coupling. *J. Ship Res.* 2, 36–46.

yton Jones, J. C. & Cancaya, I. 1997 A note on th

in regular beam seas. *J. Ship Res.* 41, 224–229.

ston, T. ⁸. Stewart, L. 1978, Stability of ships. I
- Poston, T. & Stewart, I. 1978 Stability of ships. In *Catastrophe theory and its applications*, ch. 10. Boston, MA: Pitman. Poston, I. & Stewart, I. 1978 Stability of ships. In Catastrophe theory and its applications,
ch. 10. Boston, MA: Pitman.
Rainey, R. C. T. & Thompson, J. M. T. 1991 Transient capsize diagram—a new method of
quantifying st
- ch. 10. Boston, MA: Pitman.
iney, R. C. T. & Thompson, J. M. T. 1991 Transient
quantifying stability in waves. *J. Ship Res.* 35, 58–62.
poinboldt. W. C. 1986 Numerical analysis of parameteria Rainey,R. C. T. & Thompson, J. M. T. 1991 Transient capsize diagram—a new metho-

quantifying stability in waves. *J. Ship Res.* **35**, 58–62.

Rheinboldt, W. C. 1986 *Numerical analysis of parameterized nonlinear equation*
-
- quantifying stability in waves. *[J.](http://pippo.ingentaselect.com/nw=1/rpsv/cgi-bin/linker?ext=a&reqidx=/0022-4502^28^2926L.246[aid=540314,csa=0022-4502^26vol=26^26iss=4^26firstpage=246]) Ship Res.* **33**, 38–62.
Rheinboldt, W. C. 1986 Numerical analysis of parameterized nonlinear equations. Wiley.
Roberts, J. B. 1982 Effect of parametric excitation on ship rolling motion Roberts, J. B. 1982 Effect of parametric excitation on ship rolling motion in random waves. *J. Ship Res.* **26**, 246–253. Sanchez,S. B. 1962 Effect of parametric excitation on sinp rolling motion in random waves. J.
Ship Res. 26, 246–253.
Sanchez, N. E. & Nayfeh, A. H. 1990 Nonlinear rolling motions of ships in longitudinal waves.
Int. Shiph
- *Intip Res.* **26**, 246–253.
 Int. Shipbuilding Progr. 37, 247–272.
 Int. Shipbuilding Progr. 37, 247–272.
 Andlin T. E., Ling. T. & Shame, S. D. Sanchez, N. E. & Nayten, A. H. 1990 Nonlinear rolling motions of ships in longitudinal waves.
 Int. Shipbuilding Progr. 37, 247–272.

Schellin, T. E., Jiang, T. & Sharma, S. D. 1990 Motion simulation and dynamic stabili
- Int. Shipbuilding Progr. 37, 247–272.
hellin, T. E., Jiang, T. & Sharma, S. D. 1990 Motion simulation and dynamic stability of an
anchored tanker subject to current, wind and waves. *Ship Technol. Res. Schiffstechnik* 37,
 anchored tanker subject to current, wind and waves. *Ship Technol. Res. Schiffstechnik* 37, 64–84.
Scolan, Y. M. 1998 Technical note on ship rolling associated to high degree polynomial restoring
- moment by using the Melnikov method. *Appl. Ocean Res.* 19, 225–234. Scolan,Y. M. 1998 Technical note on ship rolling associated to high degree polynomial restoring
moment by using the Melnikov method. *Appl. Ocean Res.* **19**, 225–234.
Senjanović, 1994 Harmonic analysis of nonlinear oscill
- moment by using tr
njanović, 1994 Harn
Res. 29, 112–126.
thne B. B. & Pajaj Sethna,P. R. & Bajaj, A. K. 1978 Bifurcations in dynamical systems with internal resonance.
Sethna, P. R. & Bajaj, A. K. 1978 Bifurcations in dynamical systems with internal resonance.
 $\frac{4 \text{ SME}}{4 \text{ N}} \frac{1 \text{ and } Mech}$ \frac
- *Res.* **29**, 112–126.
thna, P. R. & Bajaj, A. K. 1978 Bifur
ASME J. Appl. Mech. **45**, 895–902.
udal B. 1988 Fram could britten to cha Seydel, R. 1988 *From equilibrium to chaos. Practical bifurcarion and stability analysis*. Elsevier.
-
- Seydel, R. 1988 From equilibrium to chaos. Practical bifurcarion and stability analysis. Elsevier.
Sharma, S. D., Jiang, T. & Schellin, T. E. 1988 Dynamic instability and chaotic motions of a
single-point moored tanker. In ydel, R. 1988 *From equilibrium to chaos. Practical bifurcarion and stability analysis.* Elsevier.
arma, S. D., Jiang, T. & Schellin, T. E. 1988 Dynamic instability and chaotic motions of a
single-point moored tanker. In single-point moored tanker. In *Proc. 17th ONR Symp. on Naval Hydrodynamics*, pp. 543–563.
Spyrou, K. J. 1990 A new approach for assessing ship manoeuvrability based on dynamical sys-
- tems' theory. PhD thesis, Department of Ship and Marine Technology, University of Strathclyde.
- Spyrou, K. J. 1995 Surf-riding, yaw instability and large heeling of ships in following/quartering waves. *Ship Technol. Res. Schiffstechnik* 42, 103-112. Spyrou, K. J. 1995 Surf-riding, yaw instability and large heeling of ships in following/quartering
waves. *Ship Technol. Res. Schiffstechnik* 42, 103–112.
Spyrou, K. J. 1996a Dynamic instability in quartering seas: the be
- waves. *Ship Technol. Res. Schiffstecl*
yrou, K. J. 1996a Dynamic instabil
broaching. *J. Ship Res.* 40, 46–59.
yrou, K. J. 1906k Homoglinic connect Spyrou, K. J. 1996a Dynamic instability in quartering seas: the behaviour of a ship during
broaching. J. Ship Res. 40, 46–59.
Spyrou, K. J. 1996b Homoclinic connections and period doublings of a ship advancing in quar-
te
- tering *J. Ship Kes.* **40**, 46–59.

yrou, K. J. 1996b Homoclinic cont

tering waves. *Chaos* **6**, 209–218. teringwaves. *Chaos* 6, 209–218.
Spyrou, K. J. 1996c Dynamic instability in quartering seas. Part II. Analysis of ship roll and
- capsize for broaching. *J. Ship Res.* 40, 326-336.
- Spyrou, K. J. 1997a Dynamic instability in quartering seas. Part III. Nonlinear effects on periodic motions. *J. Ship Res.* 41, 210-223. Spyrou, K. J. 1997a Dynamic instability in quartering seas. Part III. Nonlinear effects on periodic
motions. J. Ship Res. 41, 210–223.
Spyrou, K. J. 1997b A new method to analyse escape phenomena in multi-degree dynamics,

- motions. *J. Ship Res.* 41, 210–223.
yrou, K. J. 1997b A new method to analyse escape phenomena in multi-degree dynamics,
applied to the broaching problem. In *Proc. 6th Int. Conf. on Stability of Ships and Ocean*
Vehicles *Vehicles, Varna, Bulgaria, September 1997, vol. I, pp. 83–91.*
 Vehicles, Varna, Bulgaria, September 1997, vol. I, pp. 83–91.
 Vehicles, Varna, Bulgaria, September 1997, vol. I, pp. 83–91. applied to the broaching problem. In *Proc. 6th Int. Conf. on Stability of Ships and Ocean Vehicles, Varna, Bulgaria, September 1997*, vol. I, pp. 83–91.
Spyrou, K. J. 2000 Designing against parametric instability in follo
-
- Thompson, J. M. T. 1996 Global dynamics of driven oscillators: fractal basins and indeterminate bifurcations. In *Nonlinear mathematics* and *its applications*: fractal basins and indetermi-
nate bifurcations. In *Nonlinear mathematics and its applications* (ed. P. Aston). Cambridge
University Press Expression, J. M. T.

1 Iniversity Press.

1 M. T. nate biturcations. In *Nonunear mathematics and its applications* (ed. P. Aston). Cambridge
University Press.
Thompson, J. M. T. 1997 Designing against capsize in beam seas: recent advances and new
insights Anal Mech Rev.
- University Press.

iompson, J. M. T. 1997 Designing agains

insights. *Appl. Mech. Rev.* 50, 307–325.

compson, J. M. T. & Bishon, S. B. (eds) 19
- insights. *Appl. Mech. Rev.* 50, 307–325.
Thompson, J. M. T. & Bishop, S. R. (eds) 1994 *Nonlinearity and chaos in engineering dynamics*.
Wiley.
- Thompson, J. M. T. & de Souza, J. R. 1996 Suppression of escape by resonant modal interactions in shell vibration and heave-roll capsize. *Proc. R. Soc. Lond.* A 452, 2527-2550. Thompson, J. M. T. & de Souza, J. K. 1996 Suppression of escape by resonant modal interactions
in shell vibration and heave-roll capsize. *Proc. R. Soc. Lond.* A 452, 2527–2550.
Thompson, J. M. T. & MacMillen, F. B. J. (e
- in shell vibration and heave–roll capsize. *Proc. R. Soc. Lond.* A 452, 2527–2550.
compson, J. M. T. & MacMillen, F. B. J. (eds) 1998 Nonlinear flight dynamics
performance aircraft. Theme Issue of *Phil. Trans. R. Soc. Lon* performanceaircraft. Theme Issue of *Phil. Trans. R. Soc. Lond.* **356**, 2163–2333.
Thompson, J. M. T. & Soliman, M. S. 1990 Fractal control boundaries of driven oscillators and
- their relevance to safe engineering design. *Proc. R. Soc. Lond.* A 428, 1–13.
- Thompson, J. M. T. & Stewart, H. B. 1986 *Nonlinear dynamics and chaos*. Wiley.
- Thompson, J. M. T., Rainey, R. C. T. & Soliman, M. S. 1992 Mechanics of ship capsize under direct and parametric wave excitation. *Phil. Trans. R. Soc. Lond.* A 428, 1-13. Thompson, J. M. T., Kamey, K. C. T. & Soliman, M. S. 1992 Mechanics of ship capsize under
direct and parametric wave excitation. *Phil. Trans. R. Soc. Lond.* A 428, 1–13.
Thompson, J. M. T., Stewart, H. B. & Ueda, Y. 1994
- direct and parametric wave excitation. *Phil. Trans. R. Soc. Lon* compson, J. M. T., Stewart, H. B. & Ueda, Y. 1994 Safe, explosive in dissipative dynamical systems. *Phys. Rev.* E49, 1019–1027. indissipative dynamical systems. *Phys. Rev.* E49, 1019–1027.
Troesch, A. W. & Falzarano, J. M. 1993 Modern nonlinear dynamical analysis of vertical plane
- roll motion of planing hulls. *J. Ship Res.* 37, 189-199.
- Umeda, N. 1990 Probabilistic studyonsurf-ridingofaship in irregular following seas. In *Proc.* 4th Int. Conf. on Stability of Ships and Ocean Vehicles, STAB '90, Naples, Italy, pp. 336–343.
- Umeda, N. 1990 Probabilistic study on surf-riding of a ship in irregular following seas. In Proc.

4th Int. Conf. on Stability of Ships and Ocean Vehicles, STAB '90, Naples, Italy, pp. 336–343.

Virgin, L. N. 1987 The non 4th Int. Conf. on Stability of Ships and Ocean Vehicles, regin, L. N. 1987 The nonlinear rolling response of a ves
to capsize in regular seas. *Appl. Ocean Res.* 9, 89–95.
abbab. B. & Swaan, W. A. 1964 Coursekooping and br Virgin,L. N. 1987 The nonlinear rolling response of a vessel including chaotic motions leading
to capsize in regular seas. *Appl. Ocean Res.* 9, 89–95.
Wahab, R. & Swaan, W. A. 1964 Coursekeeping and broaching of ships in
- to capsize in regular
ahab, R. & Swaan,
Ship Res. 7, 1–15.
abouson, J. V. 1979. ShipRes. 7, 1–15.
Wehausen, J. V. 1979 Ship theory, ship design and Georg Weinblum. *Schiffstechnik* 26, 174–178.
-
- Wellicome, J. F. 1975 An analytical study of the mechanism of capsizing. In *Proc. 1st Int. Conf. on Stability of Ships and Ocean Vehicles, University of Strathclyde, Glasgow*. Wiggins, S. 1991 *Chaotic transport in dynamical systems*. Springer.
-
- on staoutry of ships and Ocean Venicies, University of Strathciyae, Glasgow.
Wiggins, S. 1991 Chaotic transport in dynamical systems. Springer.
Wright, J. H. G. & Marshfield, W. B. 1980 Ship roll response and capsize behav iggins, S. 1991 *Chaotic transport in*

right, J. H. G. & Marshfield, W. B

seas. *Trans. RINA* 122, 129–148.

oman F. C. 1977 Catestrophe theor Zeeman, E. C. 1977 *Catastrophe theory*. Reading, MA: Addison-Wesley.
-